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INVESTIGATION OF CONCRETE MATERIALS
FOR FELSENTHAL AND "CALION" LOCKS
AND DAMS, OUACHITA AND BLACK RIVERS
ARKANSAS AND LOUISIANA

by

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August 1965

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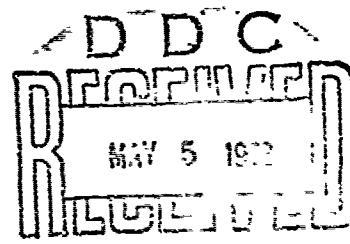
Conducted for

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Vicksburg

by

Lower Mississippi Valley Division
Materials and Concrete Laboratory

U. S. Army Engineer Waterways Experiment Station
CORPS OF ENGINEERS
Vicksburg, Mississippi



31

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Foreword

The investigation covered by this report was authorized on 12 August 1964 by letter from the District Engineer, U. S. Army Engineer District, Vicksburg, Mississippi, subject, "Ouachita and Black Rivers, Arkansas and Louisiana - Funds for Laboratory Tests."

The work was performed at the Lower Mississippi Valley Division (LMVD) Materials and Concrete Laboratory, U. S. Army Engineer Waterways Experiment Station (WES), under the direction of Mr. Thomas E. Kennedy, and under the supervision of Mrs. Katherine Mather and Messrs. Leonard Pepper and R. L. Curry. The report was prepared by Mr. Curry and Mr. Alan D. Buck.

Directors of WES during the investigation and the preparation of this report were Col. Alex G. Sutton, Jr., CE, and Col. John R. Oswalt, Jr., CE. Technical Director was Mr. J. B. Tiffany.

Contents

| | <u>Page</u> |
|---|-------------|
| Foreword | iii |
| Summary | vii |
| Introduction | 1 |
| Materials | 1 |
| Tests | 2 |
| Results, Conclusions, and Recommendations | 3 |
| Results | 3 |
| Conclusions | 3 |
| Recommendations | 4 |
| Tables 1-3 | |
| Plates 1-17 | |
| Appendix A: Petrographic Report | A1 |
| Tables A1-A5 | |

Summary

In this investigation natural sand and gravel from five sources and water from two sources were tested for suitability for use in making concrete to be used in construction of Felsenthal and Calion Locks and Dams.

The results of the tests show that the aggregates from all of the sources are potentially reactive with the alkali in cement and would therefore require the use of low-alkali cement. The coarse aggregates from the St. Francis, Pine Bluff, and Ouachita sources showed high sulfate soundness losses, but these losses seemed susceptible of reduction by thorough washing of the aggregates in water. The percentage of clay in the sand from the Monroe source was high, and this sand would also require thorough washing. The mortar-making properties test of the Pine Bluff sand indicated low strength percentages when the sand was tested as received, but the strength was satisfactory when the sand was tested after washing in water. The absorption was high on one of the Pine Bluff gravel samples. The water samples were satisfactory for use as mixing water in concrete.

It is recommended that all of the sources tested be listed as sources from which acceptable aggregate can be produced for the Felsenthal and Calion Locks and Dams, but that it be required that the material actually produced for use on these projects be graded and processed in such a manner as to meet the project specification requirements and that the absorption be less than 1.5 percent.

INVESTIGATION OF CONCRETE MATERIALS FOR FELSENTHAL AND
CALION LOCKS AND DAMS, OUACHITA AND BLACK RIVERS
ARKANSAS AND LOUISIANA

Introduction

1. This investigation was undertaken to evaluate aggregates for possible use in the construction of Felsenhal and Calion projects and possible future structures on the Ouachita and Black Rivers in Arkansas and Louisiana. The results of the investigation will form a part of "Design Memorandum No. 23 - Availability of Construction Materials, Felsenhal and Calion Locks and Dams."

Materials

2. Samples of natural fine and coarse aggregates were obtained from five sources, as follows:

| Vicksburg District Source No. | WES Concrete Division Serial No. | Producer, Location | Type of Sample |
|--|---|--|---|
| 8 | VICKS-26 S-1(2) G-1(4) | Ouachita Aggregate Co., Inc. Hampton, Ark. | Natural sand and No. 4 to 1-1/2-in. gravel |
| 12 | VICKS-26 S-2(2) G-2(2) | St. Francis Materials Co. Harrell, Ark. | Natural sand and No. 4 to 1-in. gravel |
| 11 | LR-18 S-1(2) VICKS-23 G-1(2) G-1(3) | Pine Bluff Sand and Gravel Co. Pine Bluff, Ark. | Natural sand, No. 4 to 1-1/2-in. gravel, and sup- plemental gravel sample |
| 13 | VICKS-39 S-3 G-3 | Standard Gravel Co. Camden, Ark. | Natural sand and No. 4 to 1-in. gravel |
| -- | VICKS-39 S-2 G-2 | Monroe Sand and Gravel Co. Sterlington, La. | Natural sand and No. 4 to 1-1/2-in. gravel, and 1/2- to 2-in. gravel |

3. Concrete mixing water samples were received from two sources, as follows:

| WES Concrete Division Serial No. | Location |
|-------------------------------------|---|
| VICKS-39 W-1 | Ouachita River, approximately 1 mile east of Calion Lock and Dam site |
| VICKS-39 W-2 | In Grand Marais Lake, approximately 2 miles south of Felsenthal Lock and Dam site |

Tests

4. The materials were tested as follows:

- a. Gravel and sand from each source were subjected to petrographic analysis by method CRD-C 127.*
- b. Each size group of aggregate from each source was tested for reactivity with sodium hydroxide by the quick chemical method, CRD-C 128.
- c. Coarse and fine aggregates from each source were subjected to the following tests: sieve analysis (CRD-C 103); bulk specific gravity, saturated surface dry (CRD-C 107 or 108); absorption (CRD-C 107 or 108); soundness using magnesium sulfate (CRD-C 115); and clay lumps (CRD-C 118).
- d. Coarse aggregate from each source was tested for soft particles (CRD-C 130), percent lighter than 2.40 specific gravity (CRD-C 122), percent flat and elongated particles (CRD-C 119), and Los Angeles abrasion loss (CRD-C 117).
- e. Fine aggregate from each source was tested for organic impurities (CRD-C 121), percent lighter than 2.00 specific gravity (CRD-C 122), and mortar-making properties, i.e. compressive strength (CRD-C 115).
- f. Fine Bluff sand and gravel were subjected to the following additional tests. A sample of the sand which was thoroughly washed in water to remove the fine silt was tested for mortar-making properties. The supplemental sample of the gravel, obtained at the site of production from which Felsenthal and Calion aggregates would be shipped, VICKS-23 G-1(3), was tested for magnesium sulfate soundness and Los Angeles abrasion loss.
- g. The two water samples were tested for suitability for use in mixing concrete (CRD-C 406).

* U. S. Army Engineer Waterways Experiment Station, CE, Handbook for Concrete and Cement, with quarterly supplements (Vicksburg, Miss., August 1949).

5. Sand and gravel from Ouachita Aggregate Co. and St. Francis Material: No. had been previously tested for use as construction materials for the Calion Pumping Station, and Pine Bluff sand and gravel for use in the Flat Bayou Drainage Structure. Results of those tests are included in the data reported herein.

Results, Conclusions, and Recommendations

Results

6. The test results are given at the end of this report in the following manner:

- a. The results of the petrographic examination of the coarse and fine aggregate samples are reported in Appendix A and tables A1-A5.
- b. Results of the chemical tests for reactivity of aggregate with sodium hydroxide are reported in plates 1-4.
- c. Aggregate test data are reported in plates 5-12 and in table 1.
- d. Results of the magnesium sulfate soundness tests of the aggregates are reported in plates 13-17.
- e. Results of the tests of the two water samples are reported in tables 2 and 3.

Conclusions

7. The conclusions derived from this investigation are as follows:

- a. Since one fine aggregate (LR-18 S-1) and all but one (VICKS-26 C-1(2)) of the coarse aggregates showed potential reactivity with sodium hydroxide, low-alkali cement should be used in concrete containing aggregates from the sources tested in this study.
- b. The aggregate from each source will have to be regraded to meet Corps of Engineers Guide Specification grading requirements for concrete aggregate.
- c. The Monroe sand will require washing to remove objectionable quantities of clay.
- d. The Pine Bluff, St. Francis, and Ouachita aggregates will require washing and selective processing to insure that satisfactory sand and gravel are obtained from these sources. The high percentage loss in the sulfate soundness test of unwashed gravel, the low strengths of mortars containing unwashed sand, and the high Los Angeles abrasion loss of the unwashed gravel all showed improvement when washed samples

were tested. The 2.4 percent absorption of the latest shipment of Pine Bluff gravel appeared undesirably high, but the 1.2 percent absorption of the previous shipment indicates that properly selected and processed gravel from this source would have a satisfactory percent absorption.

- e. Based on the strengths of mortars made using the test water samples, water from these two sources would be satisfactory for use as mixing water in concrete.

Recommendations

8. It is recommended that all of the sources given in paragraph 2 be listed as sources from which acceptable aggregate can be produced for the Felsenthal and Calion Locks and Dams, but that it be required that the material actually produced for use on these projects be graded and processed in such a manner as to meet the project specification requirements and that the absorption be less than 1.5 percent.

Table I
Results of Tests of Fine and Coarse Aggregates

| Source | Sample Designation | Coarse and Fine Aggregates | | | | Coarse Aggregate | | | | Fine Aggregate | | | |
|--------------------------------------|--|----------------------------|-------------------------------|--------------------|--------------------------------|---------------------------------------|-----------------------------------|------------------------------------|--------------------|--|----------------------|---|--|
| | | Bulk Sp Gr USD | Absorp- tion Yield % | Clay Lumps % | Reactive Clay Yield % | Soft Parti- cles, % Meth. | Lighter than 2.40 Sp Gr., % | Flat and Elongated Sp Gr., % | LA Particles, % | Organic Impurities than 2.00 Sp Gr., %* | Lighter Sp Gr., % | Compressive Strength, 3 Day 7 Day | |
| Monroe Sand and Gravel Co. | VICKS-39 G-2 1/2 to 2 in. No. 4 to 1-1/2 in. | 2.55 | 1.2 | 0.1 | Yes | 0.0 | 6.8 | 2.8 | 21.2 | -- | -- | -- | |
| | VICKS-39 G-2 | 2.55 | 1.3 | 0.1 | Yes | 0.0 | 7.2 | 2.6 | 21.2 | -- | -- | -- | |
| Standard Gravel Co. | VICKS-39 G-3 | 2.57 | 1.3 | 0.1 | Yes | 0.0 | 6.6 | 3.7 | 25.5 | -- | -- | -- | |
| | VICKS-39 G-3 | 2.62 | 0.5 | 0.0 | No | -- | -- | -- | -- | 3 | 0.0 | 125 | |
| Ouachita Aggregate Co. | VICKS-26 G-1(4) | 2.57 | 1.4 | 0.1 | Yes | 0.0 | 2.5 | 2.7 | 29.8 | -- | -- | -- | |
| | VICKS-26 G-1(2) | 2.61 | 0.7 | 0.1 | No | -- | -- | -- | -- | 1 | 0.0 | 125 | |
| Porous Shipments | VICKS-26 G-1(2) | 2.58 | 1.3 | 0.6 | No | 0.2 | -- | 2 | 27.4 | -- | -- | -- | |
| | VICKS-26 S-1 | 2.60 | 1.0 | 0 | No | -- | -- | -- | 2 | -- | 129 | 130 | |
| St. Francis' Material Co. | VICKS-26 G-2(2) | 2.57 | 1.3 | 0.0 | Yes | 0.0 | 6.0 | 3.0 | 30.0 | -- | -- | -- | |
| | VICKS-26 S-2(2) | 2.61 | 0.6 | 0.1 | No | -- | -- | -- | -- | 0 | 0.0 | 119 109 | |
| Previous shipment | VICKS-26 G-2 | 2.56 | 1.6 | 0 | -- | 0.0 | 0 | 9 | 42 | -- | -- | -- | |
| | VICKS-26 S-2 | 2.62 | 0.6 | 0.8 | -- | 1 | -- | -- | 2 | -- | 119 | 120 | |
| Pine Bluff Sand and Gravel Co. | VICKS-23 G-1(2) | 2.54 | 2.4 | 0.1 | Yes | 0.0 | 8.8 | 2.0 | 36.0 | -- | -- | -- | |
| | LR-18 S-1(2) | 2.60 | 0.9 | 0.4 | No | -- | -- | -- | -- | 1 | 0.0 | 78 89 | |
| Supplemen- tal ship- ment | LR-18 S-1(2) weather | -- | -- | 10.4 | -- | -- | -- | -- | 30.1 | -- | -- | -- | |
| | VICKS-23 G-1(3) | -- | -- | -- | -- | -- | -- | -- | -- | -- | 114 | 112 | |
| Previous shipment | VICKS-23 G-1 | 2.56 | 1.4 | 7.8 | -- | Yes | 0.0 | 4.6 | 28.2 | -- | -- | -- | |
| | TR-18 S-1 | 2.60 | 0.7 | -- | Yes | -- | -- | -- | -- | -- | -- | -- | |

* Water-making properties of the fine aggregate are indicated by the compressive strength values.
** This refers to the organic impurity figure used in the test (CRD-C 121).

Table 2

Results of Tests of Water Sample VICKS-39 W-1 for Use in Mixing Concrete

Source of Sample: Guachita River, approximately 1 mile east of Calion Lock and Dam site

Test Method Used: CRD-C 406 Cement Used: Marquette Type III

| Test Age days | Compressive Strength of Specimens Containing Test Water in Percent of Strength of Specimens Containing Distilled Water | |
|------------------|---|-------------------|
| | Test Result | Specified Minimum |
| 3 | 102 | 90 |
| 7 | 99 | 90 |

Table 3

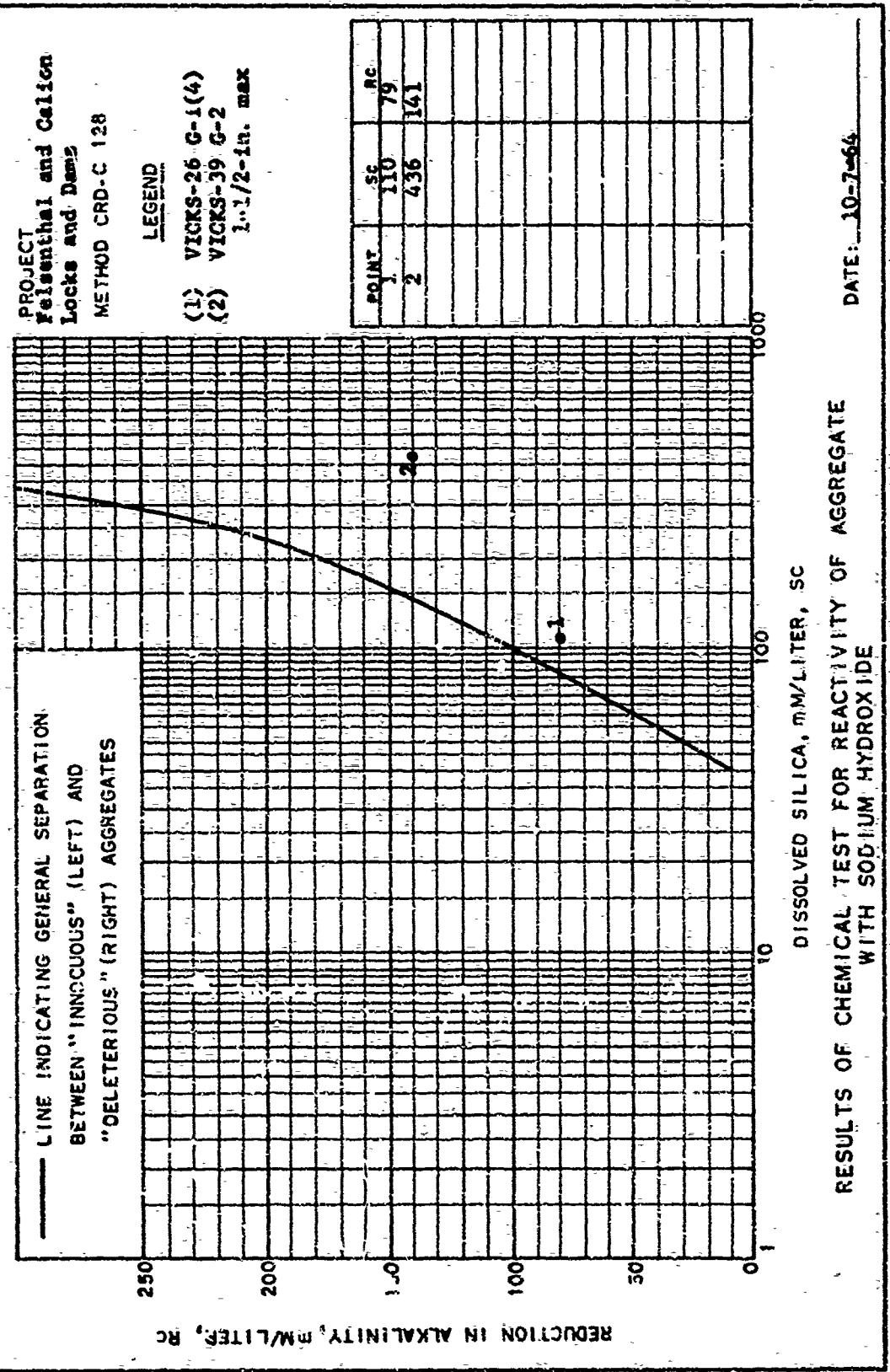
Results of Tests of Water Sample VICKS-39 W-2 for Use in Mixing Concrete

Source of Sample: Grand Marais Lake, approximately two miles south of Felsenthal Lock and Dam site

Test Method Used: CRD-C 406 Cement Used: Marquette Type III

| Test Age days | Compressive Strength of Specimens Containing Test Water in Percent of Strength of Specimens Containing Distilled Water | |
|------------------|---|-------------------|
| | Test Result | Specified Minimum |
| 3 | 91 | 90 |
| 7 | 91 | 90 |

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PLATE I

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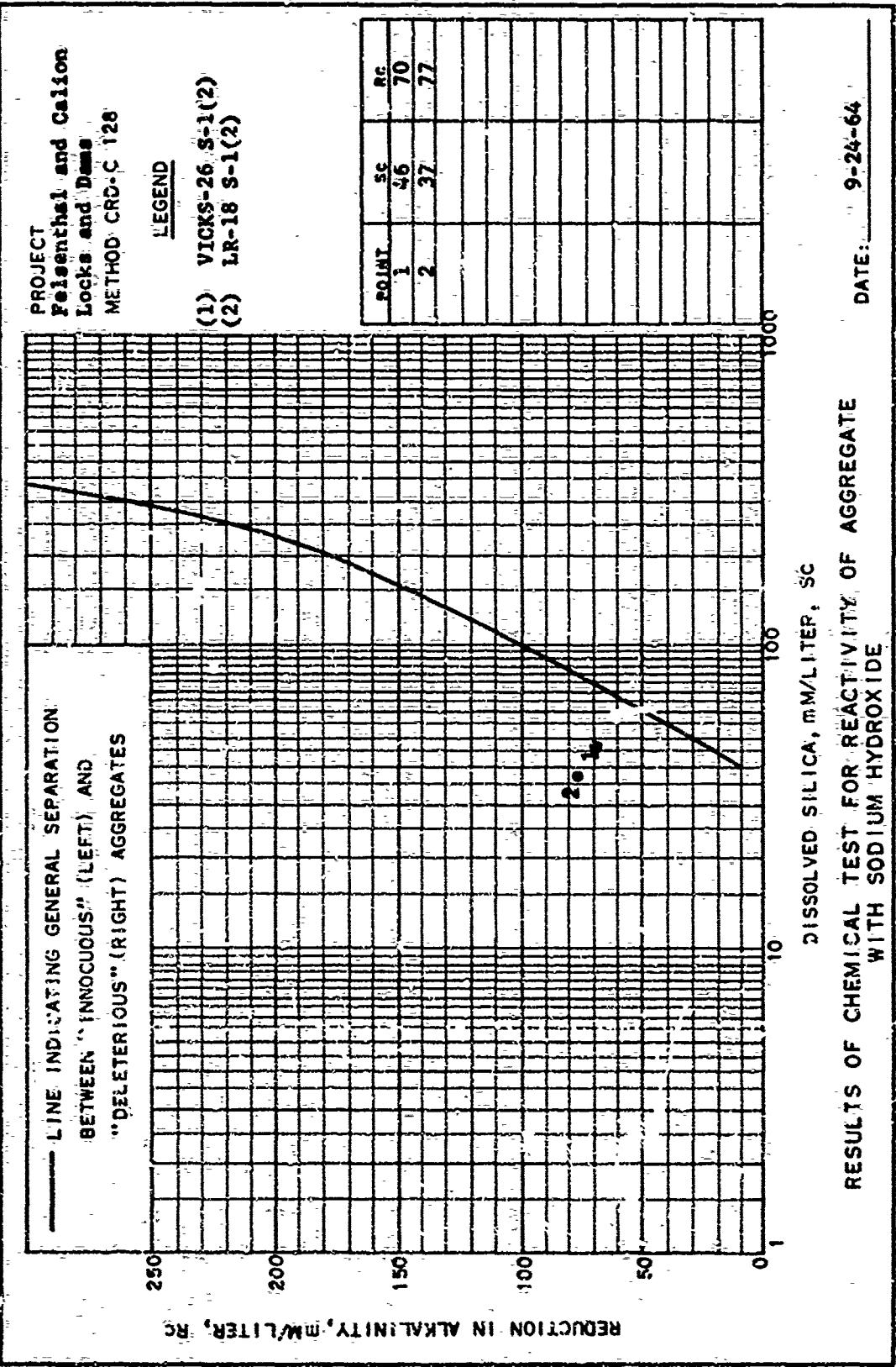


PLATE 2

CORPS OF ENGINEERS, U. S. ARMY, Lower Miss. Valley Division.

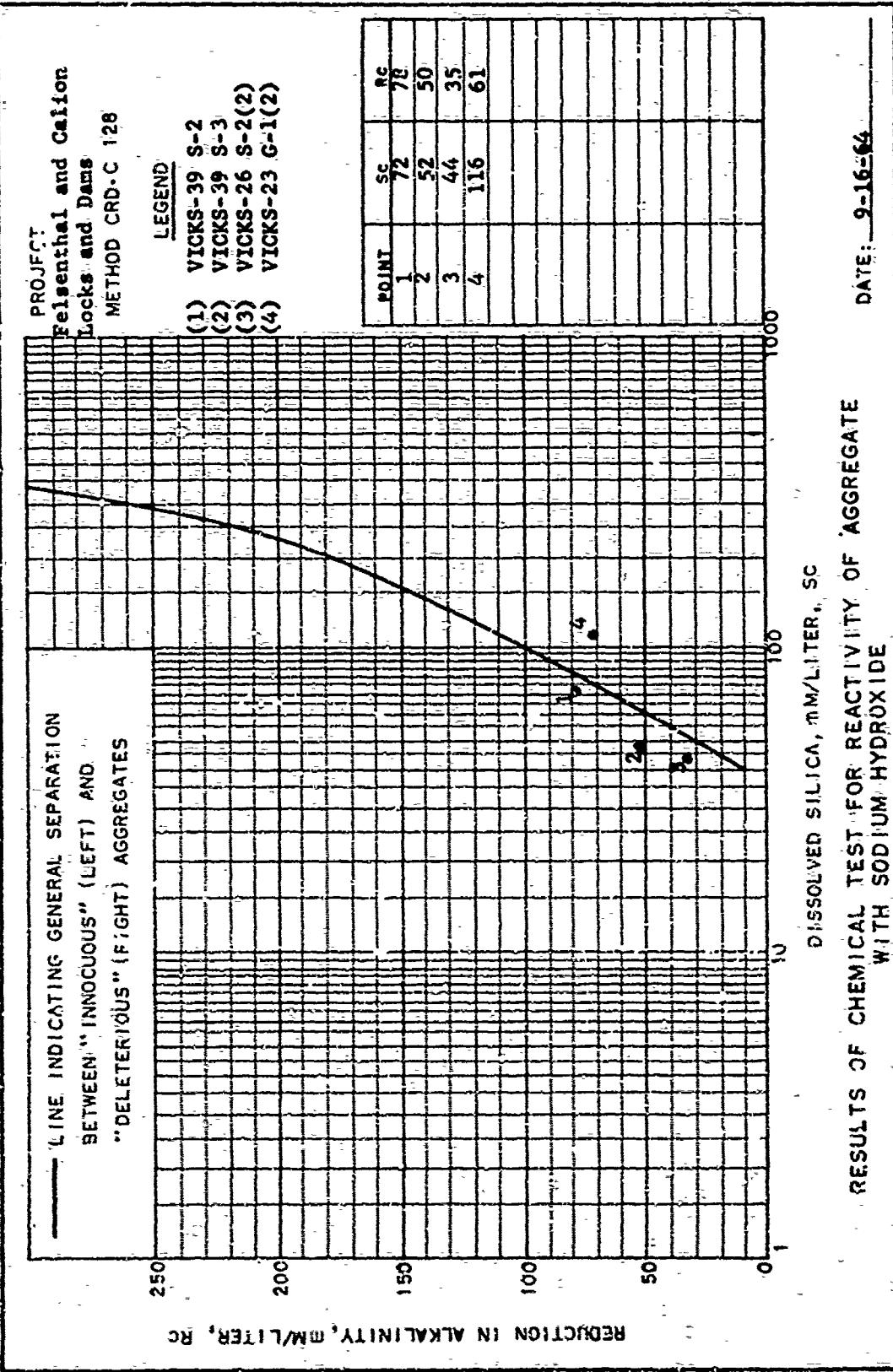
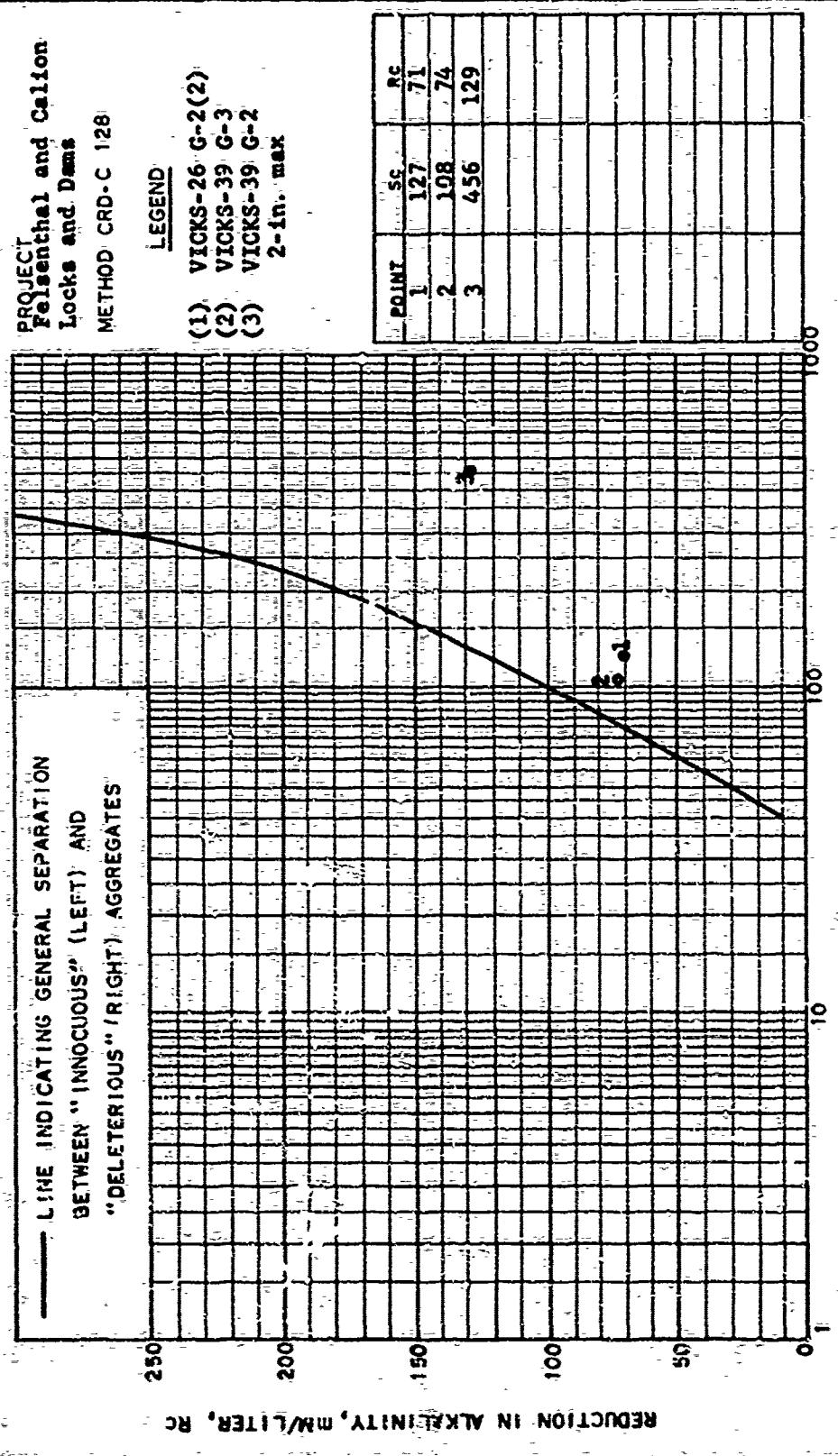


PLATE 3

ARMY. - U.S. CORPS OF ENGINEERS. SECRETARIES. VALLEY DIVISION.

LIE INDICATING GENERAL SEPARATION BETWEEN "INNOCUOUS" (LEFT) AND "DELETERIOUS" (RIGHT) AGGREGATES

PROJECT
Felsenthal and Callion
Locks and Dams
METHOD CRD.C 128



RESULTS OF CHEMICAL TEST FOR REACTIVITY OF AGGREGATE WITH SODIUM HYDROXIDE

DATE: 9-29-64

WES FORM 896

| STATE: Ark. | INDEX NO.: | AGGREGATE | TESTED BY: USAEWES | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| LAT: 33 | LONG: 92 | DATA SHEET | DATE: Nov 1964 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| LAB SYMBOL NO: VICKS-26 S-2(2), G-2(2) | | TYPE OF MATERIAL: Nat. sand and gravel | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| LOCATION: 3 miles north of Harrell, Ark. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| PRODUCER: St. Francis Materials Co. (Harrell's Pit), Harrell, Ark., Vickshire District Source No. 12 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SAMPLED BY: USAEWES | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| TESTED FOR: Felsenthal and Calion Locks and Dams | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| PROCESSING BEFORE TESTING: None | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| GEOLOGICAL FORMATION AND AGE: | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1"> <thead> <tr> <th colspan="4">GRADING (CRD-C 105)(CUM. % PASSING):</th> <th colspan="5">TEST RESULTS</th> </tr> <tr> <th>SIEVE</th> <th>3-8"</th> <th>1&-3"</th> <th>2-1&"</th> <th>1&-1&"</th> <th>1&-1&"</th> <th>1&-1&"</th> <th>1&-1&"</th> <th>1&-1&"</th> <th>FINE AGG.</th> </tr> </thead> <tbody> <tr> <td>SIEVE</td> <td>3-8"</td> <td>1&-3"</td> <td>2-1&"</td> <td>1&-1&"</td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>6IN.</td> <td></td> <td></td> <td></td> <td></td> <td>BULK SP. GR., SAT SURF. DRY (CRD-C 107,108):</td> <td></td> <td></td> <td></td> <td>2.572.61</td> </tr> <tr> <td>5IN.</td> <td></td> <td></td> <td></td> <td></td> <td>ABSORPTION, PER CENT (CRD-C 107,108):</td> <td></td> <td></td> <td></td> <td>1.3 0.6</td> </tr> <tr> <td>4IN.</td> <td></td> <td></td> <td></td> <td></td> <td>ORGANIC IMPURITIES, FIG. NO. (CRD-C 12):</td> <td></td> <td></td> <td></td> <td>0</td> </tr> <tr> <td>3IN.</td> <td></td> <td></td> <td></td> <td></td> <td>SOFT PARTICLES, PER CENT (CRD-C 130):</td> <td></td> <td></td> <td></td> <td>0.0</td> </tr> <tr> <td>2&1/2IN.</td> <td></td> <td></td> <td></td> <td></td> <td>PER CENT LIGHTER THAN SP. GR.: 4.0 (CRD-C 122):</td> <td></td> <td></td> <td></td> <td>8.0</td> </tr> <tr> <td>2IN.</td> <td></td> <td></td> <td></td> <td></td> <td>PER CENT FLAT AND ELONGATED (CRD-C 119,120):</td> <td></td> <td></td> <td></td> <td>3.0</td> </tr> <tr> <td>1&1/2IN.</td> <td></td> <td></td> <td></td> <td>100</td> <td>WEIGHTED AV. % LOSS, 5 CYC. M35.5-1, 2, 3, 4, 5 (CRD-C 110):</td> <td></td> <td></td> <td></td> <td>*12.06.0</td> </tr> <tr> <td>1IN.</td> <td></td> <td></td> <td></td> <td>95</td> <td>ABRASION LOSS (L.A.), %, (CRD-C 117):</td> <td></td> <td></td> <td></td> <td>30.0</td> </tr> <tr> <td>1&1/2IN.</td> <td></td> <td></td> <td></td> <td>71</td> <td>UNIT WT., LB./CU FT (CRD-C 106):</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>1IN.</td> <td></td> <td></td> <td></td> <td>38</td> <td>CLAY LUMPS, % (CRD-C 118):</td> <td></td> <td></td> <td></td> <td>0.00.1</td> </tr> <tr> <td>1&1/2IN.</td> <td></td> <td></td> <td></td> <td>18</td> <td>PER CENT LIGHTER THAN SP. GR. 2.00 (CRD-C 122):</td> <td></td> <td></td> <td></td> <td>0.0</td> </tr> <tr> <td>NO.4</td> <td></td> <td></td> <td>1 100</td> <td></td> <td>SPECIFIC HEAT, BTU/LB/DEG. F. (CRD-C 124):</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>NO.8</td> <td></td> <td></td> <td>86</td> <td></td> <td>REACTIVITY WITH NaOH (CRD-C 126): 3c, mM/L</td> <td></td> <td></td> <td></td> <td>127 44</td> </tr> <tr> <td>NO.16</td> <td></td> <td></td> <td>70</td> <td></td> <td>* R_c, mM/L</td> <td></td> <td></td> <td></td> <td>71 35</td> </tr> <tr> <td>NO.30</td> <td></td> <td></td> <td>60</td> <td></td> <td>MORTAR-MAKING PROPERTIES (CRD-C 116):</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>NO.50</td> <td></td> <td></td> <td>23</td> <td></td> <td>TYPE III CEMENT, RATIO 3 DAYS, 110 %, 7 DAYS, 100 %</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>NO.100</td> <td></td> <td></td> <td>1</td> <td></td> <td>LINEAR THERMAL EXPANSION X10 9 DEG. F. (CRD-C 125,126):</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>NO.200</td> <td></td> <td></td> <td>--</td> <td></td> <td>ROCK TYPE</td> <td>PARALLEL</td> <td>ACROSS</td> <td>ON</td> <td>AVERAGE</td> </tr> <tr> <td>- 200"</td> <td></td> <td></td> <td>0.4</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>F.M.^(a)</td> <td></td> <td></td> <td>2.60</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td colspan="4">(a) CRD-C 105 (b) CRD-C 104</td> <td colspan="5">MORTAR:</td> </tr> <tr> <td colspan="4">MORTAR-CEM EXPANSION AT 100F, % (CRD-C 123):</td> <td colspan="4">FINE AGGREGATE</td> <td colspan="2">COARSE AGGREGATE</td> </tr> <tr> <td colspan="4">LOW-ALK. CEMENT: % Na₂O EQUIVALENT:</td> <td>3 MO.</td> <td>5 MO.</td> <td>8 MO.</td> <td>12 MO.</td> <td>3 MO.</td> <td>5 MO.</td> <td>8 MO.</td> <td>12 MO.</td> </tr> <tr> <td colspan="4">HIGH-ALK. CEMENT: % Na₂O EQUIVALENT:</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td colspan="4">SOUNDNESS IN CONCRETE (CRD-C 40,114):</td> <td></td> <td></td> <td></td> <td></td> <td>T & T</td> <td>HW-CD</td> <td>HD-CW</td> </tr> <tr> <td colspan="4">FINE AGG.</td> <td>COARSE AGG:</td> <td></td> <td></td> <td>DFT₂₀₀</td> <td></td> <td></td> <td></td> </tr> <tr> <td colspan="4">FINE AGG.</td> <td>COARSE AGG:</td> <td></td> <td></td> <td>DFT₃₀₀</td> <td></td> <td></td> <td></td> </tr> <tr> <td colspan="12">PETROGRAPHIC DATA (CRD-C 127): Percentage Composition</td> </tr> <tr> <td colspan="4">Constituents</td> <td colspan="4">Gravel</td> <td colspan="4">Sand</td> </tr> <tr> <td>Chert</td> <td></td> <td></td> <td></td> <td>82</td> <td></td> <td></td> <td></td> <td>26</td> <td></td> <td></td> <td></td> </tr> <tr> <td>Quartz</td> <td></td> <td></td> <td></td> <td>17</td> <td></td> <td></td> <td></td> <td>73</td> <td></td> <td></td> <td></td> </tr> <tr> <td>Sandstone, quartzite, and assorted rock types</td> <td></td> <td></td> <td></td> <td>1</td> <td></td> <td></td> <td></td> <td>1</td> <td></td> <td></td> <td></td> </tr> <tr> <td colspan="12">REMARKS: * The gravel shows a possibility of deleterious reactivity if used with a high-alkali cement. Sulfate soundness loss high.</td> </tr> </tbody></table> | | | | GRADING (CRD-C 105)(CUM. % PASSING): | | | | TEST RESULTS | | | | | SIEVE | 3-8" | 1&-3" | 2-1&" | 1&-1&" | 1&-1&" | 1&-1&" | 1&-1&" | 1&-1&" | FINE AGG. | SIEVE | 3-8" | 1&-3" | 2-1&" | 1&-1&" | | | | | | 6IN. | | | | | BULK SP. GR., SAT SURF. DRY (CRD-C 107,108): | | | | 2.572.61 | 5IN. | | | | | ABSORPTION, PER CENT (CRD-C 107,108): | | | | 1.3 0.6 | 4IN. | | | | | ORGANIC IMPURITIES, FIG. NO. (CRD-C 12): | | | | 0 | 3IN. | | | | | SOFT PARTICLES, PER CENT (CRD-C 130): | | | | 0.0 | 2&1/2IN. | | | | | PER CENT LIGHTER THAN SP. GR.: 4.0 (CRD-C 122): | | | | 8.0 | 2IN. | | | | | PER CENT FLAT AND ELONGATED (CRD-C 119,120): | | | | 3.0 | 1&1/2IN. | | | | 100 | WEIGHTED AV. % LOSS, 5 CYC. M35.5-1, 2, 3, 4, 5 (CRD-C 110): | | | | *12.06.0 | 1IN. | | | | 95 | ABRASION LOSS (L.A.), %, (CRD-C 117): | | | | 30.0 | 1&1/2IN. | | | | 71 | UNIT WT., LB./CU FT (CRD-C 106): | | | | | 1IN. | | | | 38 | CLAY LUMPS, % (CRD-C 118): | | | | 0.00.1 | 1&1/2IN. | | | | 18 | PER CENT LIGHTER THAN SP. GR. 2.00 (CRD-C 122): | | | | 0.0 | NO.4 | | | 1 100 | | SPECIFIC HEAT, BTU/LB/DEG. F. (CRD-C 124): | | | | | NO.8 | | | 86 | | REACTIVITY WITH NaOH (CRD-C 126): 3c, mM/L | | | | 127 44 | NO.16 | | | 70 | | * R _c , mM/L | | | | 71 35 | NO.30 | | | 60 | | MORTAR-MAKING PROPERTIES (CRD-C 116): | | | | | NO.50 | | | 23 | | TYPE III CEMENT, RATIO 3 DAYS, 110 %, 7 DAYS, 100 % | | | | | NO.100 | | | 1 | | LINEAR THERMAL EXPANSION X10 9 DEG. F. (CRD-C 125,126): | | | | | NO.200 | | | -- | | ROCK TYPE | PARALLEL | ACROSS | ON | AVERAGE | - 200" | | | 0.4 | | | | | | | F.M. ^(a) | | | 2.60 | | | | | | | (a) CRD-C 105 (b) CRD-C 104 | | | | MORTAR: | | | | | MORTAR-CEM EXPANSION AT 100F, % (CRD-C 123): | | | | FINE AGGREGATE | | | | COARSE AGGREGATE | | LOW-ALK. CEMENT: % Na ₂ O EQUIVALENT: | | | | 3 MO. | 5 MO. | 8 MO. | 12 MO. | 3 MO. | 5 MO. | 8 MO. | 12 MO. | HIGH-ALK. CEMENT: % Na ₂ O EQUIVALENT: | | | | | | | | | | | | SOUNDNESS IN CONCRETE (CRD-C 40,114): | | | | | | | | T & T | HW-CD | HD-CW | FINE AGG. | | | | COARSE AGG: | | | DFT ₂₀₀ | | | | FINE AGG. | | | | COARSE AGG: | | | DFT ₃₀₀ | | | | PETROGRAPHIC DATA (CRD-C 127): Percentage Composition | | | | | | | | | | | | Constituents | | | | Gravel | | | | Sand | | | | Chert | | | | 82 | | | | 26 | | | | Quartz | | | | 17 | | | | 73 | | | | Sandstone, quartzite, and assorted rock types | | | | 1 | | | | 1 | | | | REMARKS: * The gravel shows a possibility of deleterious reactivity if used with a high-alkali cement. Sulfate soundness loss high. | | | | | | | | | | | |
| GRADING (CRD-C 105)(CUM. % PASSING): | | | | TEST RESULTS | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SIEVE | 3-8" | 1&-3" | 2-1&" | 1&-1&" | 1&-1&" | 1&-1&" | 1&-1&" | 1&-1&" | FINE AGG. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SIEVE | 3-8" | 1&-3" | 2-1&" | 1&-1&" | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6IN. | | | | | BULK SP. GR., SAT SURF. DRY (CRD-C 107,108): | | | | 2.572.61 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 5IN. | | | | | ABSORPTION, PER CENT (CRD-C 107,108): | | | | 1.3 0.6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 4IN. | | | | | ORGANIC IMPURITIES, FIG. NO. (CRD-C 12): | | | | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3IN. | | | | | SOFT PARTICLES, PER CENT (CRD-C 130): | | | | 0.0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2&1/2IN. | | | | | PER CENT LIGHTER THAN SP. GR.: 4.0 (CRD-C 122): | | | | 8.0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2IN. | | | | | PER CENT FLAT AND ELONGATED (CRD-C 119,120): | | | | 3.0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1&1/2IN. | | | | 100 | WEIGHTED AV. % LOSS, 5 CYC. M35.5-1, 2, 3, 4, 5 (CRD-C 110): | | | | *12.06.0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1IN. | | | | 95 | ABRASION LOSS (L.A.), %, (CRD-C 117): | | | | 30.0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1&1/2IN. | | | | 71 | UNIT WT., LB./CU FT (CRD-C 106): | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1IN. | | | | 38 | CLAY LUMPS, % (CRD-C 118): | | | | 0.00.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1&1/2IN. | | | | 18 | PER CENT LIGHTER THAN SP. GR. 2.00 (CRD-C 122): | | | | 0.0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| NO.4 | | | 1 100 | | SPECIFIC HEAT, BTU/LB/DEG. F. (CRD-C 124): | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| NO.8 | | | 86 | | REACTIVITY WITH NaOH (CRD-C 126): 3c, mM/L | | | | 127 44 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| NO.16 | | | 70 | | * R _c , mM/L | | | | 71 35 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| NO.30 | | | 60 | | MORTAR-MAKING PROPERTIES (CRD-C 116): | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| NO.50 | | | 23 | | TYPE III CEMENT, RATIO 3 DAYS, 110 %, 7 DAYS, 100 % | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| NO.100 | | | 1 | | LINEAR THERMAL EXPANSION X10 9 DEG. F. (CRD-C 125,126): | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| NO.200 | | | -- | | ROCK TYPE | PARALLEL | ACROSS | ON | AVERAGE | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| - 200" | | | 0.4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| F.M. ^(a) | | | 2.60 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| (a) CRD-C 105 (b) CRD-C 104 | | | | MORTAR: | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| MORTAR-CEM EXPANSION AT 100F, % (CRD-C 123): | | | | FINE AGGREGATE | | | | COARSE AGGREGATE | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| LOW-ALK. CEMENT: % Na ₂ O EQUIVALENT: | | | | 3 MO. | 5 MO. | 8 MO. | 12 MO. | 3 MO. | 5 MO. | 8 MO. | 12 MO. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| HIGH-ALK. CEMENT: % Na ₂ O EQUIVALENT: | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SOUNDNESS IN CONCRETE (CRD-C 40,114): | | | | | | | | T & T | HW-CD | HD-CW | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| FINE AGG. | | | | COARSE AGG: | | | DFT ₂₀₀ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| FINE AGG. | | | | COARSE AGG: | | | DFT ₃₀₀ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| PETROGRAPHIC DATA (CRD-C 127): Percentage Composition | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Constituents | | | | Gravel | | | | Sand | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Chert | | | | 82 | | | | 26 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Quartz | | | | 17 | | | | 73 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Sandstone, quartzite, and assorted rock types | | | | 1 | | | | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| REMARKS: * The gravel shows a possibility of deleterious reactivity if used with a high-alkali cement. Sulfate soundness loss high. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

WES FORM 726 JAN. 1951

PLATE 5

| | | | | | | | | | | | | |
|--|-----------------|--|---------------------|------|-----------------|--|----------|--------|--------------------|---------|-----------|--------|
| STATE: ARK. | INDEX NO.: | AGGREGATE DATA SHEET | TESTED BY: USAEWE'S | | | | | | | | | |
| LAT.: 33 | LONG.: 92 | | DATE: Nov 1964 | | | | | | | | | |
| LAB. SYMBOL NO.: VICKS-39 S-3, G-3 | | TYPE OF MATERIAL: Nat. sand and gravel | | | | | | | | | | |
| LOCATION: Just north of Camden, Ark., north of Hwy 79 on Gravel Pit Road | | | | | | | | | | | | |
| PRODUCER: Standard Gravel Co., Camden, Ark., Vicksburg District Source No. 13 | | | | | | | | | | | | |
| SAMPLED BY: USAEWE'S | | | | | | | | | | | | |
| TESTED FOR: Folsomthal and Calion Locks and Dams | | | | | | | | | | | | |
| PROCESSING BEFORE TESTING: | | | | | | | | | | | | |
| GEOLOGICAL FORMATION AND AGE: | | | | | | | | | | | | |
| GRADING (CRD-C 109)(CUM. % PASSING): | | | | | TEST RESULTS | | | | | | | |
| SIEVE | 3-6" | 1½-3" | ½-1½" | ½-1" | FINE AGG. | | 3-6" | 1½-3" | ½-1½" | ½-1" | FINE AGG. | |
| 6 IN. | | | | | | BULK SP. GR., SAT. SURF DRY (CRD-C 107,108): | | | | | 2.572 62 | |
| 5 IN. | | | | | | ABSORPTION, PER CENT (CRD-C 107,108): | | | | | 1.3 0.5 | |
| 4 IN. | | | | | | ORGANIC IMPURITIES, FIG. NO. (CRD-C 121): | | | | | 3 | |
| 3 IN. | | | | | | SOFT PARTICLES, PER CENT (CRD-C 130): | | | | | 0.0 | |
| 2½ IN. | | | | | | PER CENT LIGHTER THAN SP. GR. 2.40 (CRD-C 122): | | | | | 6.6 | |
| 2 IN. | | | | | | PER CENT FLAT AND ELONGATED (CRD-C 119,120): | | | | | 3.7 | |
| 1½ IN. | | | | 100 | | WEIGHTED AV. % LOSS, 5 CYC. MgSO ₄ (1/2 - 1/2 - 1/2) (CRD-C 115): | | | | | 4.1 3.2 | |
| 1 IN. | | | 95 | | | ABRASION LOSS (L.A.), % (CRD-C 117): | | | | | 26.5 | |
| ¾ IN. | | 81 | | | | UNIT WT., LB/CU FT (CRD-C 106): | | | | | | |
| ½ IN. | 46 | | | | | CLAY LUMPS, % (CRD-C 118): | | | | | 0.0 0.0 | |
| NO. 4 | 16 | | | | | PER CENT LIGHTER THAN SP. GR. 2.00 (CRD-C 122): | | | | | | |
| NO. 8 | 0 | 100 | | | | SPECIFIC HEAT, BTU/LB/DEG. F. (CRD-C 124): | | | | | | |
| NO. 16 | 88 | | | | | REACTIVITY WITH NaOH (CRD-C 128): Sc, MM/L: | | | | | 106.52 | |
| NO. 30 | 81 | | | | | * Sc, MM/L: | | | | | 74.50 | |
| NO. 50 | 75 | | | | | MORTAR-MAKING PROPERTIES (CRD-C 116): | | | | | | |
| NO. 100 | 33 | | | | | TYPE III CEMENT, RATIO 3 DAYS, 125 % 7 DAYS, 125 % | | | | | | |
| NO. 200 | | | | | | LINEAR THERMAL EXPANSION 210 °DEG. F. (CRD-C 125,126): | | | | | | |
| -200 ⁽⁶⁾ | | | 0.3 | | | ROCK TYPE | PARALLEL | ACROSS | ON | AVERAGE | | |
| F.M. ⁽⁶⁾ | | | 2.20 | | | | | | | | | |
| (a) CRD-C 105 (b) CRD-C 104 | | | | | MORTAR: | | | | | | | |
| VOLATILE-PAIR EXPANSION AT 100%, % (CRD-C 123): | | | | | FINE AGGREGATE | | | | COARSE AGGREGATE | | | |
| LOW-ALK. CEMENT: % Na ₂ O EQUIVALENT: | | | | | 3 MO. | 6 MO. | 9 MO. | 12 MO. | 3 MO. | 6 MO. | 9 MO. | 12 MO. |
| HIGH-ALK. CEMENT: % Na ₂ O EQUIVALENT: | | | | | | | | | | | | |
| SOUNDNESS IN CONCRETE (CRD-C 40,114): | | | | | | | | | | | | |
| FINE AGG. COARSE AGG: | | | | | | | | | DPE ₃₀₀ | | | |
| FINE AGG. COARSE AGG: | | | | | | | | | DPE ₂₀₀ | | | |
| PETROGRAPHIC DATA (CRD-C 127): Percentage Composition (some chalcedonic chert in sand) | | | | | | | | | | | | |
| Gravel | | | | | | | | | | | | |
| Constituents | 3/4 - 1-1/2 in. | | | | No. 4 - 3/4 in. | | | | Sand | | | |
| Chert | 92 | | | | 90 | | | | 27 | | | |
| Quartz | 7 | | | | 8 | | | | 69 | | | |
| Sandstone, quartzite, and assorted rock types | 1 | | | | 2 | | | | 4 | | | |
| REMARKS: * The gravel shows a possibility of deleterious reactivity if used with a high-alkali cement. | | | | | | | | | | | | |

| STATE: ARK. | INDEX NO.: | AGGREGATE DATA SHEET | TESTED BY: USAEWEIS | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|--|---|--|---------------------|-----------------|-----------------------|--------------|--------|------------------|-----------------------|--------------|--------|--------|----------|-----------|-------|--|--|--|--|------|------|-------|---------------------------------------|--|--|--|-----|-----|-------|---|--|--|--|---|---|-------|---------------------------------------|--|--|--|-----|---|-----------|---|--|--|--|-----|---|-------|---|--|--|--|-----|---|-----------|--|--|--|--|------|------|-------|--|--|--|--|------|------|---------|----------------------------------|--|--|--|---|---|---------|----------------------------|--|--|--|-----|-----|---------|---|--|--|--|---|-----|-------|--|--|--|--|---|---|-------|-----------------------------------|--|--|--|----------|-----|----|--------|--|--|--|--|----------|----|----|--------|---|--|--|--|---|---|---|--------|--|--|--|--|---|---|---|---------|---------|--|--|--|-----------|----------|--------|----|---------|---------|--|--|--|--|---|---|---|---|---|--------|--|--|--|--|---|---|---|---|---|------|--|--|--|--|---|---|---|---|---|-----------------------------|--|--|--|--|---|---|---|---|---|---|--|--|--|----------------|--|--|--|------------------|--|--|--|--|--|-------|-------|-------|--------|-------|-------|-------|--------|---|--|--|--|---|---|---|---|---|---|---|---|--|--|--|--|--|--|--|--|-------|---------|---------|-----------|--|--|--|--------------|--|--|--|---------|---|---|-----------|--|--|--|--------------|--|--|--|---------|---|---|--|--|--|--|--|--|--|--|--|--|--------|--|--|--|--|--|--|--|--|--|--------------|-----------------|--|--|-----------------|--|--|------|--|--|-------|----|--|--|----|--|--|----|--|--|--------|----|--|--|----|--|--|----|--|--|--|-------|--|--|---|--|--|---|--|--|---|--|--|--|--|--|--|--|--|--|
| LAT.: 33 | LONG: 92 | | DATE: Nov. 1964 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| LAB. SYMBOL NO.: L.R-18 S-1(2); VICKS-23 G-1(2), G-2(3) | | TYPE OF MATERIAL: Nat. sand and gravel | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| LOCATION: 1/4 to 1/2 mile south of Hwy 79 on gravel crossroad, approximately 2-1/2 miles west of Bearden, Ark. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| PRODUCER: Pine Bluff Sand and Gravel Co., Pine Bluff, Ark., Vicksburg District Source No. 11 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SAMPLED BY: USAEWEIS | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| TESTED FOR: Felsenenthal and Calion Locks and Dams | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| PROCESSING BEFORE TESTING: None | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| GEOLOGICAL FORMATION AND AGE: GRADING (CRD-C 103)(CLM. % PASSING): <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th rowspan="2">SIEVE</th> <th colspan="4">TEST RESULTS</th> <th rowspan="2">DE WAXED SAMPLE</th> <th rowspan="2">FINE AGG.</th> </tr> <tr> <th>3-6"</th> <th>1/2-3"</th> <th>1/8-1/2"</th> <th>1/16-1/8"</th> </tr> </thead> <tbody> <tr> <td>6 IN.</td> <td colspan="4">BULK SP. GR., Saturated Surface Dry (CRD-C 107,108):</td> <td>2.54</td> <td>2.60</td> </tr> <tr> <td>5 IN.</td> <td colspan="4">ABSORPTION, PER CENT (CRD-C 107,108):</td> <td>2.4</td> <td>0.9</td> </tr> <tr> <td>4 IN.</td> <td colspan="4">ORGANIC IMPURITIES, FIG. NO. (CRD-C 121):</td> <td>—</td> <td>—</td> </tr> <tr> <td>3 IN.</td> <td colspan="4">SOFT PARTICLES, PER CENT (CRD-C 130):</td> <td>0.0</td> <td>—</td> </tr> <tr> <td>2 1/2 IN.</td> <td colspan="4">PER CENT LIGHTER THAN SP. GR. 2.40 (CRD-C 122):</td> <td>8.8</td> <td>—</td> </tr> <tr> <td>2 IN.</td> <td colspan="4">PER CENT FLAT AND ELONGATED (CRD-C 19,120):</td> <td>2.0</td> <td>—</td> </tr> <tr> <td>1 1/2 IN.</td> <td colspan="4">WEIGHTED AVERAGE % LOSS, 5 CYC. $MgSO_4$ (1/2-1", 1/4-1/2") (CRD-C 115):</td> <td>18.7</td> <td>19.4</td> </tr> <tr> <td>1 IN.</td> <td colspan="4">ABRASION LOSS (L. A.), %, (CRD-C 117):</td> <td>30.1</td> <td>36.0</td> </tr> <tr> <td>1/2 IN.</td> <td colspan="4">UNIT WT., LB./CU FT (CRD-C 106):</td> <td>—</td> <td>—</td> </tr> <tr> <td>1/4 IN.</td> <td colspan="4">CLAY LUMPS, % (CRD-C 116):</td> <td>0.1</td> <td>0.4</td> </tr> <tr> <td>1/8 IN.</td> <td colspan="4">PER CENT LIGHTER THAN SP. GR. 2.00 (CRD-C 122):</td> <td>—</td> <td>0.0</td> </tr> <tr> <td>NO. 4</td> <td colspan="4">SPECIFIC HEAT, BTU/LB/DEG. F. (CRD-C 124):</td> <td>—</td> <td>—</td> </tr> <tr> <td>NO. 8</td> <td colspan="4">REACTIVITY WITH NaOH (CRD-C 128):</td> <td>Sc, mM/L</td> <td>316</td> <td>37</td> </tr> <tr> <td>NO. 16</td> <td colspan="4"></td> <td>Rc, mM/L</td> <td>61</td> <td>77</td> </tr> <tr> <td>NO. 30</td> <td colspan="4">MORTAR-MAKING PROPERTIES (CRD-C 118): III TYPE WASHED CEMENT, RATIO 5 : 1, 78 DAYS, 7 : 1, 7 DAYS, 60 : 1, 112 %</td> <td>—</td> <td>—</td> <td>—</td> </tr> <tr> <td>NO. 50</td> <td colspan="4">LINEAR THERMAL EXPANSION X10^-6 DEG. F. (CRD-C 125,126):</td> <td>—</td> <td>—</td> <td>—</td> </tr> <tr> <td>NO. 100</td> <td colspan="4">MORTAR:</td> <td>ROCK TYPE</td> <td>PARALLEL</td> <td>ACROSS</td> <td>ON</td> <td>AVERAGE</td> </tr> <tr> <td>NO. 200</td> <td colspan="4"></td> <td>—</td> <td>—</td> <td>—</td> <td>—</td> <td>—</td> </tr> <tr> <td>- 200"</td> <td colspan="4"></td> <td>—</td> <td>—</td> <td>—</td> <td>—</td> <td>—</td> </tr> <tr> <td>F.M.</td> <td colspan="4"></td> <td>—</td> <td>—</td> <td>—</td> <td>—</td> <td>—</td> </tr> <tr> <td>(a) CRD-C 103 (b) CRD-C 104</td> <td colspan="4"></td> <td>—</td> <td>—</td> <td>—</td> <td>—</td> <td>—</td> </tr> <tr> <td colspan="4">MORTAR-BAR EXPANSION AT 100°F, % (CRD-C 123):</td> <td colspan="4">FINE AGGREGATE</td> <td colspan="2">COARSE AGGREGATE</td> </tr> <tr> <td colspan="4">LOW-ALK. CEMENT: % Na_2O EQUIVALENT:</td> <td>3 MO.</td> <td>6 MO.</td> <td>9 MO.</td> <td>12 MO.</td> <td>3 MO.</td> <td>6 MO.</td> <td>9 MO.</td> <td>12 MO.</td> </tr> <tr> <td colspan="4">HIGH-ALK. CEMENT: % Na_2O EQUIVALENT:</td> <td>—</td> <td>—</td> <td>—</td> <td>—</td> <td>—</td> <td>—</td> <td>—</td> <td>—</td> </tr> <tr> <td colspan="4">SOUNDNESS IN CONCRETE (CRD-C 40, 114):</td> <td colspan="4"></td> <td>T & T</td> <td>H.W.-CD</td> <td>H.D.-CW</td> </tr> <tr> <td colspan="4">FINE AGG.</td> <td colspan="4">COARSE AGG.:</td> <td>DFE 300</td> <td>—</td> <td>—</td> </tr> <tr> <td colspan="4">M.S. AGG.</td> <td colspan="4">COARSE AGG.:</td> <td>DFE 300</td> <td>—</td> <td>—</td> </tr> <tr> <td colspan="10">PETROGRAPHIC DATA (CRD-C 127): Percentage Composition</td> </tr> <tr> <td colspan="10" style="text-align: center;">Gravel</td> </tr> <tr> <td>Constituents</td> <td colspan="3">3/4 - 1-1/2 in.</td> <td colspan="3">No. 4 - 3/4 in.</td> <td colspan="3">Sand</td> </tr> <tr> <td>Chert</td> <td colspan="3">89</td> <td colspan="3">86</td> <td colspan="3">34</td> </tr> <tr> <td>Quartz</td> <td colspan="3">11</td> <td colspan="3">13</td> <td colspan="3">63</td> </tr> <tr> <td>Sandstone, quartzite, and assorted rock types</td> <td colspan="3">Trace</td> <td colspan="3">1</td> <td colspan="3">3</td> </tr> <tr> <td colspan="10"> REMARKS: The gravel shows a high magnesium sulfate loss and a possibility of deleterious reactivity if used with a high-alkali cement. The sand shows low strength in mortar as compared with mortar containing standard Ottawa sand. Soundness and mortar strength were satisfactory in washed samples. </td> </tr> </tbody></table> | | | | SIEVE | TEST RESULTS | | | | DE WAXED SAMPLE | FINE AGG. | 3-6" | 1/2-3" | 1/8-1/2" | 1/16-1/8" | 6 IN. | BULK SP. GR., Saturated Surface Dry (CRD-C 107,108): | | | | 2.54 | 2.60 | 5 IN. | ABSORPTION, PER CENT (CRD-C 107,108): | | | | 2.4 | 0.9 | 4 IN. | ORGANIC IMPURITIES, FIG. NO. (CRD-C 121): | | | | — | — | 3 IN. | SOFT PARTICLES, PER CENT (CRD-C 130): | | | | 0.0 | — | 2 1/2 IN. | PER CENT LIGHTER THAN SP. GR. 2.40 (CRD-C 122): | | | | 8.8 | — | 2 IN. | PER CENT FLAT AND ELONGATED (CRD-C 19,120): | | | | 2.0 | — | 1 1/2 IN. | WEIGHTED AVERAGE % LOSS, 5 CYC. $MgSO_4$ (1/2-1", 1/4-1/2") (CRD-C 115): | | | | 18.7 | 19.4 | 1 IN. | ABRASION LOSS (L. A.), %, (CRD-C 117): | | | | 30.1 | 36.0 | 1/2 IN. | UNIT WT., LB./CU FT (CRD-C 106): | | | | — | — | 1/4 IN. | CLAY LUMPS, % (CRD-C 116): | | | | 0.1 | 0.4 | 1/8 IN. | PER CENT LIGHTER THAN SP. GR. 2.00 (CRD-C 122): | | | | — | 0.0 | NO. 4 | SPECIFIC HEAT, BTU/LB/DEG. F. (CRD-C 124): | | | | — | — | NO. 8 | REACTIVITY WITH NaOH (CRD-C 128): | | | | Sc, mM/L | 316 | 37 | NO. 16 | | | | | Rc, mM/L | 61 | 77 | NO. 30 | MORTAR-MAKING PROPERTIES (CRD-C 118): III TYPE WASHED CEMENT, RATIO 5 : 1, 78 DAYS, 7 : 1, 7 DAYS, 60 : 1, 112 % | | | | — | — | — | NO. 50 | LINEAR THERMAL EXPANSION X10^-6 DEG. F. (CRD-C 125,126): | | | | — | — | — | NO. 100 | MORTAR: | | | | ROCK TYPE | PARALLEL | ACROSS | ON | AVERAGE | NO. 200 | | | | | — | — | — | — | — | - 200" | | | | | — | — | — | — | — | F.M. | | | | | — | — | — | — | — | (a) CRD-C 103 (b) CRD-C 104 | | | | | — | — | — | — | — | MORTAR-BAR EXPANSION AT 100°F, % (CRD-C 123): | | | | FINE AGGREGATE | | | | COARSE AGGREGATE | | LOW-ALK. CEMENT: % Na_2O EQUIVALENT: | | | | 3 MO. | 6 MO. | 9 MO. | 12 MO. | 3 MO. | 6 MO. | 9 MO. | 12 MO. | HIGH-ALK. CEMENT: % Na_2O EQUIVALENT: | | | | — | — | — | — | — | — | — | — | SOUNDNESS IN CONCRETE (CRD-C 40, 114): | | | | | | | | T & T | H.W.-CD | H.D.-CW | FINE AGG. | | | | COARSE AGG.: | | | | DFE 300 | — | — | M.S. AGG. | | | | COARSE AGG.: | | | | DFE 300 | — | — | PETROGRAPHIC DATA (CRD-C 127): Percentage Composition | | | | | | | | | | Gravel | | | | | | | | | | Constituents | 3/4 - 1-1/2 in. | | | No. 4 - 3/4 in. | | | Sand | | | Chert | 89 | | | 86 | | | 34 | | | Quartz | 11 | | | 13 | | | 63 | | | Sandstone, quartzite, and assorted rock types | Trace | | | 1 | | | 3 | | | REMARKS: The gravel shows a high magnesium sulfate loss and a possibility of deleterious reactivity if used with a high-alkali cement. The sand shows low strength in mortar as compared with mortar containing standard Ottawa sand. Soundness and mortar strength were satisfactory in washed samples. | | | | | | | | | |
| SIEVE | TEST RESULTS | | | | DE WAXED SAMPLE | FINE AGG. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 3-6" | 1/2-3" | 1/8-1/2" | 1/16-1/8" | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6 IN. | BULK SP. GR., Saturated Surface Dry (CRD-C 107,108): | | | | 2.54 | 2.60 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 5 IN. | ABSORPTION, PER CENT (CRD-C 107,108): | | | | 2.4 | 0.9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 4 IN. | ORGANIC IMPURITIES, FIG. NO. (CRD-C 121): | | | | — | — | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3 IN. | SOFT PARTICLES, PER CENT (CRD-C 130): | | | | 0.0 | — | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2 1/2 IN. | PER CENT LIGHTER THAN SP. GR. 2.40 (CRD-C 122): | | | | 8.8 | — | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2 IN. | PER CENT FLAT AND ELONGATED (CRD-C 19,120): | | | | 2.0 | — | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1 1/2 IN. | WEIGHTED AVERAGE % LOSS, 5 CYC. $MgSO_4$ (1/2-1", 1/4-1/2") (CRD-C 115): | | | | 18.7 | 19.4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1 IN. | ABRASION LOSS (L. A.), %, (CRD-C 117): | | | | 30.1 | 36.0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1/2 IN. | UNIT WT., LB./CU FT (CRD-C 106): | | | | — | — | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1/4 IN. | CLAY LUMPS, % (CRD-C 116): | | | | 0.1 | 0.4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1/8 IN. | PER CENT LIGHTER THAN SP. GR. 2.00 (CRD-C 122): | | | | — | 0.0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| NO. 4 | SPECIFIC HEAT, BTU/LB/DEG. F. (CRD-C 124): | | | | — | — | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| NO. 8 | REACTIVITY WITH NaOH (CRD-C 128): | | | | Sc, mM/L | 316 | 37 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| NO. 16 | | | | | Rc, mM/L | 61 | 77 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| NO. 30 | MORTAR-MAKING PROPERTIES (CRD-C 118): III TYPE WASHED CEMENT, RATIO 5 : 1, 78 DAYS, 7 : 1, 7 DAYS, 60 : 1, 112 % | | | | — | — | — | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| NO. 50 | LINEAR THERMAL EXPANSION X10^-6 DEG. F. (CRD-C 125,126): | | | | — | — | — | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| NO. 100 | MORTAR: | | | | ROCK TYPE | PARALLEL | ACROSS | ON | AVERAGE | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| NO. 200 | | | | | — | — | — | — | — | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| - 200" | | | | | — | — | — | — | — | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| F.M. | | | | | — | — | — | — | — | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| (a) CRD-C 103 (b) CRD-C 104 | | | | | — | — | — | — | — | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| MORTAR-BAR EXPANSION AT 100°F, % (CRD-C 123): | | | | FINE AGGREGATE | | | | COARSE AGGREGATE | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| LOW-ALK. CEMENT: % Na_2O EQUIVALENT: | | | | 3 MO. | 6 MO. | 9 MO. | 12 MO. | 3 MO. | 6 MO. | 9 MO. | 12 MO. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| HIGH-ALK. CEMENT: % Na_2O EQUIVALENT: | | | | — | — | — | — | — | — | — | — | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SOUNDNESS IN CONCRETE (CRD-C 40, 114): | | | | | | | | T & T | H.W.-CD | H.D.-CW | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| FINE AGG. | | | | COARSE AGG.: | | | | DFE 300 | — | — | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| M.S. AGG. | | | | COARSE AGG.: | | | | DFE 300 | — | — | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| PETROGRAPHIC DATA (CRD-C 127): Percentage Composition | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gravel | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Constituents | 3/4 - 1-1/2 in. | | | No. 4 - 3/4 in. | | | Sand | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Chert | 89 | | | 86 | | | 34 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Quartz | 11 | | | 13 | | | 63 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Sandstone, quartzite, and assorted rock types | Trace | | | 1 | | | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| REMARKS: The gravel shows a high magnesium sulfate loss and a possibility of deleterious reactivity if used with a high-alkali cement. The sand shows low strength in mortar as compared with mortar containing standard Ottawa sand. Soundness and mortar strength were satisfactory in washed samples. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

| STATE: Ark. | INDEX NO.: | AGGREGATE | | TESTED BY: USAEWES | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|---|-----------------|---------------------------------------|---------------------|---------------------|---|----------|---------------------|---------------------|---------------------|-----------------|-----------------|--------|-------------|---------|-------|--------|---------------------|---------------------|---------------------|-----------|--|---------------------|---------------------|---------------------|--------------------|-------|--|--|--|--|---|--|--|--|--|----------|-------|--|--|--|--|---------------------------------------|--|--|--|--|--------|-------|--|--|--|--|---|--|--|--|--|---|-------|--|--|--|--|---------------------------------------|--|--|--|--|-----|---------------------|--|--|--|--|---|--|--|--|--|-----|-------|--|--|--|--|--|--|--|--|--|-----|---------------------|--|--|--|--|--|--|--|--|--|--------|-------|--|--|--|--|---------------------------------------|--|--|--|--|------|---------|--|--|--|--|---------------------------------|--|--|--|--|--|---------|--|--|--|--|----------------------------|--|--|--|--|--------|---------|--|--|--|--|---|--|--|--|--|-----|----------|--|--|--|--|--|--|--|--|--|--|------|--|--|--|--|--|--|--|--|--|-------|------|--|--|--|--|---|----------|--|--|--|------|-------|--|--|--|--|--------------------------------------|--|--|--|--|--|-------|--|--|--|--|--|--|--|--|--|--|-------|--|--|--|--|---|--|--|--|--|--|--------|--|--|--|--|---|--|--|--|--|-----------|----------|--------|----|---------|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--------|--|--|--|--|--|--|--|--|--|--|------|--|--|--|--|--|--|--|--|--|--|-------|--|--|--|--|--|--|--|--|--|--|---|--|--|--|--|--|--|--|--|--|--|-----|--|--|--|--|--|--|--|--|--|--|------|--|--|--|--|--|--|--|--|--|--|-----------------------------|--|--|--|--|---------|--|--|--|--|--|--|--|--|--|--|----------------|--|--|--|------------------|--|--|--|-------|-------|-------|--------|-------|-------|-------|--------|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|---|--|--|--|--|-----------|--|--|--|-------------|--|--|--|-------------|--|--|--|--------------------|--|--|--|-----------|--|--|--|--------------------|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|---|--|--|--|--|--|--|--|--|--|--|---|--|--|--|--|--------|--|--|--|--------------|-----------------|-----------------|------|-------|----|----|----|--------|----|----|----|--|---|-------|---|--|--|--|--|--|--|---|--|--|--|--|--|--|--|--|--|--|
| LAT: 33 | LONG: 92 | DATA SHEET | | DATE: Nov. 1964 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| LAB. SYMBOL NO.: VICKS-26 S-1(2), G-1(4) | | TYPE OF MATERIAL Nat. sand and gravel | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| LOCATION: Champagnolle Creek Deposit, 4 miles west of Hwy 167, between Hartton and El Dorado, Ark. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| PRODUCER: Ouachita Aggregate Company (Formerly Nettles Pit), Hampton, Ark. Vicksburg District Source No. 8 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SAMPLED BY: USAEWES | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| TESTED FOR: Felsenthal and Calion Locks and Dams | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| PROCESSING BEFORE TESTING: None | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| GEOLOGICAL FORMATION AND AGE: | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1"> <thead> <tr> <th colspan="5">GRADING (CRD-C 103) (CUM. % PASSING):</th> <th colspan="5">TEST RESULTS</th> </tr> <tr> <th>SIEVE</th> <th>3-6"</th> <th>1$\frac{1}{2}$-3"</th> <th>2-1$\frac{1}{2}$"</th> <th>4-1$\frac{1}{2}$"</th> <th>FINE AGG.</th> <th>3-6"</th> <th>1$\frac{1}{2}$-3"</th> <th>2-1$\frac{1}{2}$"</th> <th>4-1$\frac{1}{2}$"</th> <th>FINE AGG.</th> </tr> </thead> <tbody> <tr> <td>6 IN.</td> <td></td> <td></td> <td></td> <td></td> <td>BULK SP. GR., SAT SURF DRY (CRD-C 107,108):</td> <td></td> <td></td> <td></td> <td></td> <td>2.572.61</td> </tr> <tr> <td>5 IN.</td> <td></td> <td></td> <td></td> <td></td> <td>ABSORPTION, PER CENT (CRD-C 101,106):</td> <td></td> <td></td> <td></td> <td></td> <td>1.40.7</td> </tr> <tr> <td>4 IN.</td> <td></td> <td></td> <td></td> <td></td> <td>ORGANIC IMPURITIES, FIG. NO. (CRD-C 121):</td> <td></td> <td></td> <td></td> <td></td> <td>1</td> </tr> <tr> <td>3 IN.</td> <td></td> <td></td> <td></td> <td></td> <td>SOFT PARTICLES, PER CENT (CRD-C 130):</td> <td></td> <td></td> <td></td> <td></td> <td>0.0</td> </tr> <tr> <td>2$\frac{1}{2}$ IN.</td> <td></td> <td></td> <td></td> <td></td> <td>PER CENT LIGHTER THAN SP. GR. 2.40 (CRD-C 122):</td> <td></td> <td></td> <td></td> <td></td> <td>2.5</td> </tr> <tr> <td>2 IN.</td> <td></td> <td></td> <td></td> <td></td> <td>PER CENT FLAT AND ELONGATED (CRD-C 119,120):</td> <td></td> <td></td> <td></td> <td></td> <td>2.7</td> </tr> <tr> <td>1$\frac{1}{2}$ IN.</td> <td></td> <td></td> <td></td> <td></td> <td>WEIGHTED AV. % LOSS, 3 CYC. MgSO₄ (C 1-1, FA-1) (CRD-C 115):</td> <td></td> <td></td> <td></td> <td></td> <td>8.75.6</td> </tr> <tr> <td>1 IN.</td> <td></td> <td></td> <td></td> <td></td> <td>ABRASION LOSS (L. A.) %, (CRD-C 117):</td> <td></td> <td></td> <td></td> <td></td> <td>29.8</td> </tr> <tr> <td>1/2 IN.</td> <td></td> <td></td> <td></td> <td></td> <td>UNIT WT., LB/CU FT (CRD-C 106):</td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>1/4 IN.</td> <td></td> <td></td> <td></td> <td></td> <td>CLAY LUMPS, % (CRD-C 116):</td> <td></td> <td></td> <td></td> <td></td> <td>0.10.1</td> </tr> <tr> <td>3/8 IN.</td> <td></td> <td></td> <td></td> <td></td> <td>PER CENT LIGHTER THAN SP. GR. 2.00 (CRD-C 122):</td> <td></td> <td></td> <td></td> <td></td> <td>0.0</td> </tr> <tr> <td>5/16 IN.</td> <td></td> <td></td> <td></td> <td></td> <td>SPECIFIC HEAT, BTU/LB/DEG. F. (CRD-C 124):</td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>NO.4</td> <td></td> <td></td> <td></td> <td></td> <td>REACTIVITY WITH NaOH (CRD-C 128): Sc, mm/L</td> <td></td> <td></td> <td></td> <td></td> <td>11046</td> </tr> <tr> <td>NO.8</td> <td></td> <td></td> <td></td> <td></td> <td>*</td> <td>Rc, mm/L</td> <td></td> <td></td> <td></td> <td>7970</td> </tr> <tr> <td>NO.16</td> <td></td> <td></td> <td></td> <td></td> <td colspan="5">MORTAR-MAKING PROPERTIES (CRD-C 116)</td> <td></td> </tr> <tr> <td>NO.30</td> <td></td> <td></td> <td></td> <td></td> <td colspan="5">TYPE III CEMENT-RATIO 3 DAYS, 125 %, 7 DAYS, 121 %</td> <td></td> </tr> <tr> <td>NO.50</td> <td></td> <td></td> <td></td> <td></td> <td colspan="5">LINEAR THERMAL EXPANSION X10⁻⁶ DEG. F. (CRD-C 125,126):</td> <td></td> </tr> <tr> <td>NO.100</td> <td></td> <td></td> <td></td> <td></td> <td colspan="5"> <table border="1"> <thead> <tr> <th>ROCK TYPE</th> <th>PARALLEL</th> <th>ACROSS</th> <th>ON</th> <th>AVERAGE</th> </tr> </thead> <tbody> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> </tbody> </table> </td> <td></td> </tr> <tr> <td>NO.200</td> <td></td> <td></td> <td></td> <td></td> <td colspan="5"></td> <td></td> </tr> <tr> <td>-200</td> <td></td> <td></td> <td></td> <td></td> <td colspan="5"></td> <td></td> </tr> <tr> <td>F.M.6</td> <td></td> <td></td> <td></td> <td></td> <td colspan="5"></td> <td></td> </tr> <tr> <td>6</td> <td></td> <td></td> <td></td> <td></td> <td colspan="5"></td> <td></td> </tr> <tr> <td>1.3</td> <td></td> <td></td> <td></td> <td></td> <td colspan="5"></td> <td></td> </tr> <tr> <td>2.70</td> <td></td> <td></td> <td></td> <td></td> <td colspan="5"></td> <td></td> </tr> <tr> <td colspan="5">(a) CRD-C 105 (b) CRD-C 104</td> <td colspan="5">MORTAR:</td> <td></td> </tr> <tr> <td colspan="5"> <table border="1"> <thead> <tr> <th colspan="4">FINE AGGREGATE</th> <th colspan="4">COARSE AGGREGATE</th> </tr> <tr> <th>3 MO.</th> <th>6 MO.</th> <th>9 MO.</th> <th>12 MO.</th> <th>3 MO.</th> <th>6 MO.</th> <th>9 MO.</th> <th>12 MO.</th> </tr> </thead> <tbody> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> </tbody> </table> </td> <td colspan="5"></td> <td></td> </tr> <tr> <td colspan="5"> <table border="1"> <thead> <tr> <th colspan="4">FINE AGG.</th> <th colspan="4">COARSE AGG.</th> </tr> <tr> <th colspan="4">COARSE AGG.</th> <th colspan="4">DFE₃₀₀</th> </tr> <tr> <th colspan="4">FINE AGG.</th> <th colspan="4">DFE₃₀₀</th> </tr> </thead> <tbody> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> </tbody> </table> </td> <td colspan="5"></td> <td></td> </tr> <tr> <td colspan="5">PETROGRAPHIC DATA (CRD-C 127) Percentage Composition (Some chalcedonic chert in sand)</td> <td colspan="5"></td> <td></td> </tr> <tr> <td colspan="5"> <table border="1"> <thead> <tr> <th colspan="2">Gravel</th> <th colspan="2"></th> </tr> <tr> <th>Constituents</th> <th>3/4 - 1-1/2 in.</th> <th>No. 4 - 3/4 in.</th> <th>Sand</th> </tr> </thead> <tbody> <tr> <td>Chert</td> <td>82</td> <td>80</td> <td>27</td> </tr> <tr> <td>Quartz</td> <td>16</td> <td>20</td> <td>71</td> </tr> <tr> <td>Sandstone, quartzite, and assorted rock types</td> <td>2</td> <td>Trace</td> <td>2</td> </tr> </tbody> </table> </td> <td colspan="5"></td> <td></td> </tr> <tr> <td colspan="5">REMARKS: * The gravel shows a possibility of deleterious reactivity if used with a high-alkali cement.</td> <td colspan="5"></td> <td></td> </tr> </tbody></table> | | | | | GRADING (CRD-C 103) (CUM. % PASSING): | | | | | TEST RESULTS | | | | | SIEVE | 3-6" | 1 $\frac{1}{2}$ -3" | 2-1 $\frac{1}{2}$ " | 4-1 $\frac{1}{2}$ " | FINE AGG. | 3-6" | 1 $\frac{1}{2}$ -3" | 2-1 $\frac{1}{2}$ " | 4-1 $\frac{1}{2}$ " | FINE AGG. | 6 IN. | | | | | BULK SP. GR., SAT SURF DRY (CRD-C 107,108): | | | | | 2.572.61 | 5 IN. | | | | | ABSORPTION, PER CENT (CRD-C 101,106): | | | | | 1.40.7 | 4 IN. | | | | | ORGANIC IMPURITIES, FIG. NO. (CRD-C 121): | | | | | 1 | 3 IN. | | | | | SOFT PARTICLES, PER CENT (CRD-C 130): | | | | | 0.0 | 2 $\frac{1}{2}$ IN. | | | | | PER CENT LIGHTER THAN SP. GR. 2.40 (CRD-C 122): | | | | | 2.5 | 2 IN. | | | | | PER CENT FLAT AND ELONGATED (CRD-C 119,120): | | | | | 2.7 | 1 $\frac{1}{2}$ IN. | | | | | WEIGHTED AV. % LOSS, 3 CYC. MgSO ₄ (C 1-1, FA-1) (CRD-C 115): | | | | | 8.75.6 | 1 IN. | | | | | ABRASION LOSS (L. A.) %, (CRD-C 117): | | | | | 29.8 | 1/2 IN. | | | | | UNIT WT., LB/CU FT (CRD-C 106): | | | | | | 1/4 IN. | | | | | CLAY LUMPS, % (CRD-C 116): | | | | | 0.10.1 | 3/8 IN. | | | | | PER CENT LIGHTER THAN SP. GR. 2.00 (CRD-C 122): | | | | | 0.0 | 5/16 IN. | | | | | SPECIFIC HEAT, BTU/LB/DEG. F. (CRD-C 124): | | | | | | NO.4 | | | | | REACTIVITY WITH NaOH (CRD-C 128): Sc, mm/L | | | | | 11046 | NO.8 | | | | | * | Rc, mm/L | | | | 7970 | NO.16 | | | | | MORTAR-MAKING PROPERTIES (CRD-C 116) | | | | | | NO.30 | | | | | TYPE III CEMENT-RATIO 3 DAYS, 125 %, 7 DAYS, 121 % | | | | | | NO.50 | | | | | LINEAR THERMAL EXPANSION X10 ⁻⁶ DEG. F. (CRD-C 125,126): | | | | | | NO.100 | | | | | <table border="1"> <thead> <tr> <th>ROCK TYPE</th> <th>PARALLEL</th> <th>ACROSS</th> <th>ON</th> <th>AVERAGE</th> </tr> </thead> <tbody> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> </tbody> </table> | | | | | ROCK TYPE | PARALLEL | ACROSS | ON | AVERAGE | | | | | | | | | | | | | | | | | NO.200 | | | | | | | | | | | -200 | | | | | | | | | | | F.M.6 | | | | | | | | | | | 6 | | | | | | | | | | | 1.3 | | | | | | | | | | | 2.70 | | | | | | | | | | | (a) CRD-C 105 (b) CRD-C 104 | | | | | MORTAR: | | | | | | <table border="1"> <thead> <tr> <th colspan="4">FINE AGGREGATE</th> <th colspan="4">COARSE AGGREGATE</th> </tr> <tr> <th>3 MO.</th> <th>6 MO.</th> <th>9 MO.</th> <th>12 MO.</th> <th>3 MO.</th> <th>6 MO.</th> <th>9 MO.</th> <th>12 MO.</th> </tr> </thead> <tbody> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> </tbody> </table> | | | | | FINE AGGREGATE | | | | COARSE AGGREGATE | | | | 3 MO. | 6 MO. | 9 MO. | 12 MO. | 3 MO. | 6 MO. | 9 MO. | 12 MO. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | <table border="1"> <thead> <tr> <th colspan="4">FINE AGG.</th> <th colspan="4">COARSE AGG.</th> </tr> <tr> <th colspan="4">COARSE AGG.</th> <th colspan="4">DFE₃₀₀</th> </tr> <tr> <th colspan="4">FINE AGG.</th> <th colspan="4">DFE₃₀₀</th> </tr> </thead> <tbody> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> </tbody> </table> | | | | | FINE AGG. | | | | COARSE AGG. | | | | COARSE AGG. | | | | DFE ₃₀₀ | | | | FINE AGG. | | | | DFE ₃₀₀ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | PETROGRAPHIC DATA (CRD-C 127) Percentage Composition (Some chalcedonic chert in sand) | | | | | | | | | | | <table border="1"> <thead> <tr> <th colspan="2">Gravel</th> <th colspan="2"></th> </tr> <tr> <th>Constituents</th> <th>3/4 - 1-1/2 in.</th> <th>No. 4 - 3/4 in.</th> <th>Sand</th> </tr> </thead> <tbody> <tr> <td>Chert</td> <td>82</td> <td>80</td> <td>27</td> </tr> <tr> <td>Quartz</td> <td>16</td> <td>20</td> <td>71</td> </tr> <tr> <td>Sandstone, quartzite, and assorted rock types</td> <td>2</td> <td>Trace</td> <td>2</td> </tr> </tbody> </table> | | | | | Gravel | | | | Constituents | 3/4 - 1-1/2 in. | No. 4 - 3/4 in. | Sand | Chert | 82 | 80 | 27 | Quartz | 16 | 20 | 71 | Sandstone, quartzite, and assorted rock types | 2 | Trace | 2 | | | | | | | REMARKS: * The gravel shows a possibility of deleterious reactivity if used with a high-alkali cement. | | | | | | | | | | |
| GRADING (CRD-C 103) (CUM. % PASSING): | | | | | TEST RESULTS | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SIEVE | 3-6" | 1 $\frac{1}{2}$ -3" | 2-1 $\frac{1}{2}$ " | 4-1 $\frac{1}{2}$ " | FINE AGG. | 3-6" | 1 $\frac{1}{2}$ -3" | 2-1 $\frac{1}{2}$ " | 4-1 $\frac{1}{2}$ " | FINE AGG. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6 IN. | | | | | BULK SP. GR., SAT SURF DRY (CRD-C 107,108): | | | | | 2.572.61 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 5 IN. | | | | | ABSORPTION, PER CENT (CRD-C 101,106): | | | | | 1.40.7 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 4 IN. | | | | | ORGANIC IMPURITIES, FIG. NO. (CRD-C 121): | | | | | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3 IN. | | | | | SOFT PARTICLES, PER CENT (CRD-C 130): | | | | | 0.0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2 $\frac{1}{2}$ IN. | | | | | PER CENT LIGHTER THAN SP. GR. 2.40 (CRD-C 122): | | | | | 2.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2 IN. | | | | | PER CENT FLAT AND ELONGATED (CRD-C 119,120): | | | | | 2.7 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1 $\frac{1}{2}$ IN. | | | | | WEIGHTED AV. % LOSS, 3 CYC. MgSO ₄ (C 1-1, FA-1) (CRD-C 115): | | | | | 8.75.6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1 IN. | | | | | ABRASION LOSS (L. A.) %, (CRD-C 117): | | | | | 29.8 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1/2 IN. | | | | | UNIT WT., LB/CU FT (CRD-C 106): | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1/4 IN. | | | | | CLAY LUMPS, % (CRD-C 116): | | | | | 0.10.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3/8 IN. | | | | | PER CENT LIGHTER THAN SP. GR. 2.00 (CRD-C 122): | | | | | 0.0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 5/16 IN. | | | | | SPECIFIC HEAT, BTU/LB/DEG. F. (CRD-C 124): | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| NO.4 | | | | | REACTIVITY WITH NaOH (CRD-C 128): Sc, mm/L | | | | | 11046 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| NO.8 | | | | | * | Rc, mm/L | | | | 7970 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| NO.16 | | | | | MORTAR-MAKING PROPERTIES (CRD-C 116) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| NO.30 | | | | | TYPE III CEMENT-RATIO 3 DAYS, 125 %, 7 DAYS, 121 % | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| NO.50 | | | | | LINEAR THERMAL EXPANSION X10 ⁻⁶ DEG. F. (CRD-C 125,126): | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| NO.100 | | | | | <table border="1"> <thead> <tr> <th>ROCK TYPE</th> <th>PARALLEL</th> <th>ACROSS</th> <th>ON</th> <th>AVERAGE</th> </tr> </thead> <tbody> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> </tbody> </table> | | | | | ROCK TYPE | PARALLEL | ACROSS | ON | AVERAGE | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ROCK TYPE | PARALLEL | ACROSS | ON | AVERAGE | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| PETROGRAPHIC DATA (CRD-C 127) Percentage Composition (Some chalcedonic chert in sand) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| Chert | 82 | 80 | 27 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Quartz | 16 | 20 | 71 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Sandstone, quartzite, and assorted rock types | 2 | Trace | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| REMARKS: * The gravel shows a possibility of deleterious reactivity if used with a high-alkali cement. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

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|--|--|--|--|--------------------|
| STATE: La. | INDEX NO.: | AGGREGATE DATA SHEET | | TESTED BY: USAEWES |
| LAT: 32 | LONG: 92 | | | DATE: Nov 1964 |
| LAB. SYMBOL NO.: VICKS-39 S-2, G-2 | | TYPE OF MATERIAL: Nat. sand and gravel | | |
| LOCATION: 1/2 mile west of Sterlington, south on blacktop and gravel road | | | | |
| PRODUCER: Monroe Sand and Gravel Co., Sterlington, La. | | | | |
| SAMPLED BY: USAEWES | | | | |
| TESTED FOR: Folsomthal and Calion Locks and Dams | | | | |
| PROCESSING BEFORE TESTING: None | | | | |
| GEOLOGICAL FORMATION AND AGE: | | | | |
| GRADING (CRD-C 103) (CUM. % PASSING) | | TEST RESULTS | | |
| SIEVE | 3-6" 1 $\frac{1}{2}$ -3" 1/2-2" 1 $\frac{1}{2}$ -1 $\frac{1}{2}$ " FINE AGG. | | 3-6" 1 $\frac{1}{2}$ -3" 1/2-2" 1 $\frac{1}{2}$ -1 $\frac{1}{2}$ " FINE AGG. | |
| 6 IN. | | BULK SP. GR., SAT SURF DRY (CRD-C 107, 108): | 2.55 | 2.52 2.60 |
| 5 IN. | | ABSORPTION, PER CENT (CRD-C 107, 108): | 1.2 | 1.3 0.9 |
| 4 IN. | | ORGANIC IMPURITIES, FIG. NO. (CRD-C 121): | — | — 2 |
| 3 IN. | | SOFT PARTICLES, PER CENT (CRD-C 130): | 0.0 | 0.0 0.0 |
| 2 $\frac{1}{2}$ IN. | | PER CENT LIGHTER THAN SP. GR. 2.40 (CRD-C 122): | 6.8 | 7.2 7.2 |
| 2 IN. | | PER CENT FLAT AND ELONGATED (CRD-C 119, 120): | 2.8 | 2.6 |
| 1 $\frac{1}{2}$ IN. | 100 100 | WEIGHTED AV. % LOSS, 5 CYC. $MgSO_4$ ($\frac{1}{2}$ -1 $\frac{1}{2}$ -4- $\frac{1}{2}$) (CRD-C 115): | 2.0 | 3.2 |
| 1 IN. | 81 96 | ABRASION LOSS (L. A.) %, (CRD-C 117): | 21.2 | 21.2 21.2 |
| 5/8 IN. | 42 64 | UNIT WT., LB/CU FT (CRD-C 106): | — | — |
| 3/8 IN. | 20 38 | PER CENT LIGHTER THAN SP. GR. 2.00 (CRD-C 116): * | 0.1 | 0.1 2.2 |
| 1/2 IN. | 3 14 | COAL AND LIGNITE, % (CRD-C 122): | — | — 0.0 |
| 1/4 IN. | 6 100 | SPECIFIC HEAT, BTU/LB/DEG. F. (CRD-C 124): | — | — |
| NO. 4 | 0 02 | REACTIVITY WITH NaOH (CRD-C 128): Sc_{c} , MM/L: | 456 | 436 72 |
| NO. 8 | 81 | * Re_{c} , MM/L: | 129 | 141 78 |
| NO. 16 | 70 | MORTAR-MAKING PROPERTIES (CRD-C 116): | — | — |
| NO. 30 | 47 | TYPE III CEMENT, RATIO 3 DAYS, 133 %, 7 DAYS, 130 % | — | — |
| NO. 50 | 18 | LINEAR THERMAL EXPANSION X10 % DEG. F. (CRD-C 125, 126): | — | — |
| NO. 100 | 5 | ROCK TYPE | PARALLEL | ACROSS |
| NO. 200 | — | | 3N | AVFRACE |
| - 300 ^(a) | 2.1 | | | |
| F.M. ^(b) | 2.88 | | | |
| (a) CRD-C 105 (b) CRD-C 104 | | MORTAR: | | |
| MORTAR-BAR EXPANSION AT 100F, % (CRD-C 123): | | FINE AGGREGATE | | COARSE AGGREGATE |
| LOW-ALK. CEMENT: % Na_2O EQUIVALENT: | | 3 MO. | 5 MO. | 9 MO. 12 MO. |
| HIGH-ALK. CEMENT: % Na_2O EQUIVALENT: | | | | |
| SOUNDNESS IN CONCRETE (CRD-C 40, 114): | | | | F & T HW-CD HD-CW |
| FINE AGG. | COARSE AGG: | DFE 360 | | |
| FINE AGG. | COARSE AGG: | DFE 360 | | |
| PETROGRAPHIC DATA (CRD-C 127): Percentage Composition (some chalcedonic chert in sand) | | | | |
| Constituents | | Gravel | | |
| | | 3/4 - 1-1/2 in. | No. 4 - 3/4 in. | Sand |
| Chert | | 96 | 90 | 21 |
| Quartz | | 1 | 9 | 71 |
| Sandstone, quartzite, and assorted rock types | | 3 | 1 | 5 |
| Feldspar | | -- | -- | 3 |
| REMARKS: * The gravel shows a possibility of deleterious reactivity if used with a high-alkali cement. The percentage of clay lumps in the sand is high. | | | | |

WES FORM 726 JAN. 1951

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|--|----------------------------------|------------|-----------------------------------|
| STATE: Ark. | INDEX NO: 2(Rev #2) | AGGREGATE | TESTED BY: USAEWS |
| LAT.: 33 | LONG.: 92 | DATA SHEET | DATE: 28 March 1957, 29 Sept 1958 |
| LAB. SYMBOL NO: VICKS-26 G-1(2), S-1 Job 6001/308 | TYPE OF MATERIAL: Natural gravel | | |
| LOCATION: Pit on Nettles property, 5 mi S of Hampton, Ark., 4 mi W of Hwy 167. | | | |

PRODUCER: Ouachita Gravel Company, Nettles Pit

SAMPLED BY: Vicksburg District
TESTED FOR: Calibration Protection Works
PROCEDURE BEFORE TESTING: None

GEOLOGICAL FORMATION AND AGE: Recent Alluvial

USED IN: Calion Pumping Station (1958)

| GRADING (CRD-C 103)(CUT % PASSING) | | | TEST RESULTS | | | 3-6" | 1½-3" | ¾-1½" | ¼-¾" | FINE AGG. |
|------------------------------------|------|-------|---|----------|-----------|------|---------|-------|------|-----------|
| SIEVE | 3-6" | 1½-3" | ¾-1½" | ¼-¾" | FINE AGG. | | | | | |
| | | | BULK SP. GR., SAT SURF DRY (CRD-C 107,108): | | | | 2.58 | | 2.60 | |
| 6 IN. | | | ABSORPTION, PER CENT (CRD-C 107,108): | | | | 1.3 | | 1.0 | |
| 5 IN. | | | ORGANIC IMPURITIES, FIG. NO. (CRD-C 121): | | | | | | 2 | |
| 4 IN. | | | SOFT PARTICLES, PER CENT (CRD-C 130): | | | | 0.2 | | | |
| 3 IN. | | | PER CENT LIGHTER THAN SP. GR. (CRD-C 129): | | | | | | | |
| 2½ IN. | | | PER CENT FLAT AND ELONGATED (CRD-C 119,120): | | | | 2 | | | |
| 2 IN. | | | WEIGHTED AV. % LOSS, 5 CYC. $MgSO_4$ (1G $\frac{1}{2}$ -1, $\frac{1}{2}$ -1) (CRD-C 115): | 10.6 | | | | | 7 | |
| 1½ IN. | 100 | | ABRASION LOSS (L. A.) %, (CRD-C 117): | | | 27.1 | | | | |
| 1 IN. | 93 | | UNIT WT., LB/CU FT (CRD-C 106): | | | | | | | |
| ¾ IN. | 72 | | CLAY LUMPS, % (CRD-C 118): | | | | | | | |
| ½ IN. | 35 | | COAL AND LIGNITE, % (CRD-C 122): | | | | | | | |
| ⅓ IN. | 10 | | SPECIFIC HEAT, BTU/LB/DEG. F. (CRD-C 124): | | | | | | | |
| NO. 4 | 9 | 90 | REACTIVITY WITH NaOH (CRD-C 128): | SC, mmHg | | | 164 | | 60 | |
| NO. 8 | | 79 | | RC, mmHg | | | 178 | | 80 | |
| NO. 16 | | 60 | MORTAR-MAKING PROPERTIES (CRD-C 116): | | | | | | | |
| NO. 30 | | 40 | TYPE III CEMENT, RATIO 3 DAYS, 130 %, 7 DAYS, 130 %: | | | | | | | |
| NO. 50 | | 21 | LINEAR THERMAL EXPANSION X10 $\frac{1}{2}$ DEG. F. (CRD-C 125,126): | | | | | | | |
| NO. 100 | | 2 | ROCK TYPE | PARALLEL | ACROSS | ON | AVERAGE | | | |
| NO. 200 | | * | | | | | | | | |
| - 200 ^(a) | | 0.8 | | | | | | | | |
| F.M. ^(b) | | 2.30 | | | | | | | | |

(a) CRD-C 105 (b) CRD-C 104

MORTAR:

| MORTAR-BAR EXPANSION AT 100F, % (CRD-C 123): | FINE AGGREGATE | | | COARSE AGGREGATE | | | | |
|--|----------------|-------|-------|------------------|-------|-------|-------|--------|
| | 3 MO. | 6 MO. | 9 MO. | 12 MO. | 3 MO. | 6 MO. | 9 MO. | 12 MO. |
| LOW-ALK. CEMENT: % Na_2O EQUIVALENT: | | | | | | | | |
| HIGH-ALK. CEMENT: % Na_2O EQUIVALENT: | | | | | | | | |
| SOUNDNESS IN CONCRETE (CRD-C 40, 114): | | | | | | | | |
| FINE AGG. | COARSE AGG: | | | DFF 300 | | | | |
| FINE AGG. | COARSE AGG: | | | DFF 300 | | | | |

PETROGRAPHIC DATA (CRD-C 127):

Note (Suggested by Vicksburg District): Watch this source for a coating on the gravel; it will affect the compressive strength of concrete. Corrective action--(1) selective digging in pit and (2) effective washing.

REMARKS: Sample of No. 4 - 3/4" gravel decanted over No. 200 sieve - loss 0.5%. This sample then allowed to stand in saturated solution of oxalic acid over weekend and again decanted over No. 200. The total % passing the No. 200 sieve was then 0.9.

WFO FORM 726 JAN. 1951

PL. 10

Issued Sept 1958

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| STATE: Ark. | INDEX NO: 3 | AGGREGATE | TESTED BY: USAEWES |
| LAT.: 33 | LONG.: 92 | DATA SHEET DATE: 19 July 1957 | |
| LAB. SYMBOL NO.: VICKS-26 S-2, G-2 Job 6001/323 TYPE OF MATERIAL: Sand and gravel | | | |
| LOCATION: Harrells Pit, two miles north of Harrell, Arkansas | | | |
| PRODUCER: St. Francis Materials Company | | | |
| SAMPLED BY: Vicksburg District | | | |
| TESTED FOR: Calion Protection Works | | | |
| PROCESSING BEFORE TESTING: None | | | |
| GEOLOGICAL FORMATION AND AGE: | | | |
| USED IN: Calion Floodwall (1957) | | | |
| GRADING (CRD-C 103)(CLM. % PASSING): | | TEST RESULTS | |
| SIEVE | 3-6" 1 $\frac{1}{2}$ -3" 2-1 $\frac{1}{2}$ " 1 $\frac{1}{2}$ - $\frac{3}{4}$ " $\frac{3}{4}$ - $\frac{1}{2}$ " $\frac{1}{2}$ - $\frac{1}{4}$ " $\frac{1}{4}$ - $\frac{1}{8}$ " $\frac{1}{8}$ - $\frac{1}{16}$ " $\frac{1}{16}$ - $\frac{1}{32}$ " | FINE AGG. | |
| 6IN. | | | |
| 5IN. | | | |
| 4IN. | | | |
| 3IN. | | | |
| 2 $\frac{1}{2}$ IN. | | | |
| 2IN. | | | |
| 1 $\frac{1}{2}$ IN. | 100 | | |
| 1IN. | 55 | | |
| 2 $\frac{1}{2}$ IN. | 62 | | |
| 1IN. | 24 | | |
| 2IN. | 7 | | |
| NO 4 | 0 | SC | REACTIVITY WITH NaOH (CRD-C 126) SC, MM/L |
| NO 8 | 80 | | RC, MM/L |
| NO 16 | 5 | MORTAR-MAKING PROPERTIES (CP-C 116) | |
| NO 30 | 56 | TYPE III CEMENT, RATIO 3 DAY 119-3 7 DAYS, 120% | |
| NO 50 | 16 | LINEAR THERMAL EXPANSION X10 ⁶ DEG. F. (RD-C 125, 196) | |
| NO 100 | | WICK TEST | PARALLEL |
| NO 200 | | | |
| -200 ^(a) | 0.1 | | |
| F.M. ^(b) | 2.82 | | |
| (a) CRD-C 105 (b) CRD-C 104 MORTAR: | | | |
| MORTAR-BAR EXPANSION AT 100F, % (CRD-C 127) | | | |
| FINE AGGREGATE | | COARSE AGGREGATE | |
| LOW-ALK. CEMENT: % Na ₂ O EQUIVALENT: | 3 MO | 6 MO. | 9 MO. |
| HIGH-ALK. CEMENT: % Na ₂ O EQUIVALENT: | 12 MO. | 3 MO | 6 MO. |
| SCOUNDNESS IN CONCRETE (CRD-C 40, 114): | | F.T. | J-CD |
| FINE AGG. | COARSE AGG: | DFT 300 | |
| FINE AGG. | COARSE AGG: | DFT 300 | |
| PETROGRAPHIC DATA (CRD-C 127) | | | |
| REMARKS: | | | |

WES FORM 726 JAN. 1951

Issued Sept 1963

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|---|-----------------------|---|------------------------------|-------------|----------------|--|--------|---------|------------------|-------|--------|-------|------|-----------|--|
| STATE: Ark. | INDEX NO.: 1 (rev #2) | AGGREGATE DATA SHEET | TESTED BY: USAEWES | | | | | | | | | | | | |
| LAT.: 33 | LONG.: 92 | | DATE: 9 Feb 1956, 9 Apr 1963 | | | | | | | | | | | | |
| LAB. SYMBOL NO.: VICKS-23 G-1, Job 6001/247 | | TYPE OF MATERIAL: Bank gravel & nat. sand | | | | | | | | | | | | | |
| LOCATION: Bearder, Ark. | | LR-18 S-1, Job 6444 | | | | | | | | | | | | | |
| PRODUCER: Pine Bluff Sand and Gravel Co. | | | | | | | | | | | | | | | |
| SAMPLED BY: John Johnson, Vicksburg District | | | | | | | | | | | | | | | |
| TESTED FOR: Flat Bayou Drainage Structure | | | | | | | | | | | | | | | |
| PROCESSING BEFORE TESTING: None | | | | | | | | | | | | | | | |
| GEOLOGICAL FORMATION AND AGE: | | | | | | | | | | | | | | | |
| USED AT: Flat Bayou Drainage Structure (1956) | | | | | | | | | | | | | | | |
| GRADING (CRD-C 105)(CU. % PASSING): | | | | | | | | | | | | | | | |
| SIEVE | 3-6" | 1½-3" | ½-1½" | ¼-½" | FINER AGG. | TEST RESULTS | | | | 3-6" | 1½-3" | ½-1½" | ¼-½" | FINE AGG. | |
| 6 IN. | | | | | | BLK SP. GR., SAT SURF DRY (CRD-C 107,108): | | | | | 2.56 | | | 2.60 | |
| 5 IN. | | | | | | ABSORPTION, PER CENT (CRD-C 107,108): | | | | | 1.2 | | | 0.7 | |
| 4 IN. | | | | | | ORGANIC IMPURITIES, FIG. NO. (CRD-C 121): | | | | | | | | | |
| 3 IN. | | | | | | SOFT PARTICLES, PER CENT (CRD-C 130): | | | | | 0.0 | | | | |
| 2½ IN. | | | | | | PER CENT LIGHTER THAN SP. GR. 2.10 (CRD-C 122): | | | | | 4.6 | | | | |
| 2 IN. | | | | | | PLR. CENT. FLAT AND ELONGATED (CRD-C 119,120): | | | | | | | | | |
| 1½ IN. | | | | | | WEIGHTED. AV. % LOSS, 3 CYC. MgSO ₄ (1/2-1", 1/4-½") (CRD-C 115): | | | | | 7.8 | | | | |
| 1 IN. | | | | | | ABRASION LOSS (L. A.), %, (CRD-C 117): | | | | | 28.2 | | | | |
| 1 IN. | 91 | | | | | UNIT WT., LB/CU FT (CRD-C 106): | | | | | | | | | |
| ¾ IN. | 52 | | | | | CLAY LUMPS, % (CRD-C 118): | | | | | | | | | |
| ½ IN. | 18 | | | | | COAL AND LIGNITE, % (CRD-C 122): | | | | | | | | | |
| ⅓ IN. | 7 | | | | | SPECIFIC HEAT, BTU/LB/DEG. F. (CRD-C 124): | | | | | | | | | |
| NO. 4 | 1 | 06 | | | | REACTIVITY WITH NaOH (CRD-C 128): Sc, mm/l. | | | | | 168 | | | 168 | |
| NO. 8 | 00 | | | | | Rc, mm/l. | | | | | 89 | | | 90 | |
| NO. 16 | 76 | | | | | MORTAR-MAKING PROPERTIES (CRD-C 116) | | | | | | | | | |
| NO. 30 | 50 | | | | | TYPE: CEMENT, RATIO: DAYS: DAMP: DRY: | | | | | | | | | |
| NO. 50 | 14 | | | | | LINEAR THERMAL EXPANSION X10⁻⁶ DEG. F. (CRD-C 125,126): | | | | | | | | | |
| NO. 100 | 2 | | | | | ROCK TYPE: PARALLEL: ACROSS: ON: AVERAGE: | | | | | | | | | |
| NO. 200 | -- | | | | | | | | | | | | | | |
| - 200" | 0.7 | | | | | | | | | | | | | | |
| F.M.(b) | 2.7 | | | | | | | | | | | | | | |
| (a) CRD-C 105 (b) CRD-C 104 | MORTAR: | | | | FINE AGGREGATE | | | | COARSE AGGREGATE | | | | | | |
| MORTAR-BAR EXPANSION AT 100°F, % (CRD-C 123): | | | | 3 MO. | 6 MO. | 9 MO. | 12 MO. | 3 MO. | 6 MO. | 9 MO. | 12 MO. | | | | |
| LOW-ALK. CEMENT: % Na ₂ O EQUIVALENT: | | | | | | | | | | | | | | | |
| HIGH-ALK. CEMENT: % Na ₂ O EQUIVALENT: | | | | | | | | | | | | | | | |
| SOUNDNESS IN CONCRETE (CRD-C 4G, 116): | | | | | | | | | | | | | | | |
| FINE AGG. | | | | COARSE AGG: | | | | F.S.T | | | | HW-CD | | HD-CW | |
| FINE AGG. | | | | COARSE AGG: | | | | DFE 300 | | | | | | | |
| PETROGRAPHIC DATA (CRD-C 127): | | | | | | | | DFE 200 | | | | | | | |
| REMARKS: | | | | | | | | | | | | | | | |

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|---|---|--|
| FROM: CORPS OF ENGINEERS U. S. ARMY <u>Lower Miss. Valley DIVISION</u> | REPORT OF SOUNDNESS TEST (CRD-C 175) | ADDRESS: USAEEWES, Concrete Division P. O. Drawer 2131 Jackson, Mississippi 39205 |
| SERIAL NO. VICKS-39 Job 6606 | PROJECT Felsenthal and Calion Locks and Dams | MATERIAL Natural sand and gravel |
| SERIAL NO. VICKS-26 S-1(2), C-1(4) | SOURCE Quachita Aggregate Company, Hampton, Ark. | |

| COARSE AGGREGATE | | | | | | | | | | | |
|----------------------------|------------------------------------|---|-------|--|--------|---|-------|--|-------|--------------------------------------|-------|
| SIEVE SIZE | GRADING FOR CALCULATION (Per Cent) | WEIGHT OF TEST FRACTION BEFORE TEST (Grams) | | WEIGHT OF TEST FRACTION AFTER TEST (Grams) | | WEIGHT FINER SIEVE AFTER TEST ACTUAL LOSS (%) | | % PASSING FINER SIEVE AFTER TEST ACTUAL % LOSS | | WEIGHTED AVG CORRECTED PER CENT LOSS | |
| | | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 |
| NO. 4 TO $\frac{1}{2}$ IN. | 50 | 750 | 750 | 634.5 | 664.3 | 62.5 | 85.7 | 8.3 | 11.4 | 4.15 | 5.32 |
| $\frac{1}{2}$ TO 1 IN. | 50 | 1500 | 1500 | 1387.5 | 1385.2 | 112.5 | 114.8 | 7.5 | 7.7 | 3.75 | 3.65 |
| TOTALS | | 2250 | 2250 | 2075.0 | 2049.7 | 175.0 | 200.5 | 15.8 | 19.1 | 7.90 | 9.55 |

| CONSTITUENT (Size % to 1 in.) | NO. OF PARTICLES BEFORE TEST | | SUM WEIGHTED AVG RUNS 1 & 2 | | | | | | | | | | AVG TOTAL WEIGHTED AVG RUNS 1 & 2 | | 8.7 PER CENT | |
|----------------------------------|------------------------------------|----------|-----------------------------|----------|----------|----------|----------|--------------------------|----------|----------|----------|----------|-----------------------------------|----------|--------------|----------|
| | | | NO. PARTICLES AFTER TEST | | | | | NO. PARTICLES AFTER TEST | | | | | TOTAL | | | |
| | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 |
| Chert | 38 | 42 | 2 | 5 | 2 | 0 | 0 | 1 | 2 | 3 | 32 | 34 | 36 | 42 | | |

| | | FINE AGGREGATE | | | | | | | |
|----------------------|---|--|-------|--|-------|--|--------|--------------------------------------|----------|
| SIEVE SIZING # | GRADING FOR SLU- CULATION % | WEIGHT OF TEST FRACTIONS BEFORE TEST (Gross) | | WEIGHT OF TEST FRACTIONS AFTER TEST (Loss) | | % PASSING FINER SIEVE AFTER TEST - (Loss % Loss) | | WEIGHTED AVERAGE CORRECTED % LOSS | |
| | | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 |
| 3/8-IN.-NO. 4 | 2 | | | | | (16.2) | (18.8) | 6.3 | 0.4 |
| NO. 4-8 | 13 | 100 | 100 | 83.8 | 81.2 | 16.2 | 18.8 | 2.1 | 2.4 |
| NO. 8-16 | 20 | 100 | 100 | 94.4 | 94.2 | 5.6 | 5.8 | 1.1 | 1.2 |
| NO. 16-30 | 20 | 100 | 100 | 97.0 | 94.5 | 3.0 | 5.5 | 0.6 | 1.1 |
| NO. 30-50 | 24 | 100 | 100 | 96.6 | 95.3 | 3.4 | 4.7 | 0.8 | 1.1 |
| NO. 50-100 | 14 | - | - | - | - | 0.0 | 0.0 | 0.0 | 0.0 |
| NO. 100-PAN | 7 | - | - | - | - | 0.0 | 0.0 | 0.0 | 0.0 |
| TOTALS | 100 | 400 | 400 | 371.8 | 365.2 | 28.2 | 34.8 | 4.0 | 6.2 |
| | | SUM WEIGHTED AVG RUNS 1 & 2 | | | | | | 11.1 | |
| | | AVG TOTAL WEIGHTED AVG RUNS 1 & 2 | | | | | | 5.6 | PER CENT |

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| REMARKS | | |
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PLATE 13

| | | |
|---|--|--|
| FROM: CORPS OF ENGINEERS U. S. ARMY <u>Lower Miss. Valley</u> DIVISION | REPORT OF SOUNDNESS TEST (CRD-C 115) | ADDRESS: USAEEWES, Concrete Division P. O. Drawer 2131 Jackson, Mississippi 39205 |
| SYMBOL VICKS-39 Job 6606 | PROJECT Felsenthal and Calion Locks and Dams | MATERIAL Natural sand and gravel |
| SERIAL NO. VICKS-26 S-2(2), G-2(2) | SOURCE St. Francis Materials Company, Harrell, Ark. | |

| COARSE AGGREGATE | | | | | | | | | | | |
|------------------|---|--|-------|---|--------|--|-------|---|-------|--|-------|
| SIEVE SIZE | GRADING FOR CALCULATION (Per Cent) | WEIGHT OF TEST FRACTIONS BEFORE TEST (Grams) | | WEIGHT OF TEST FRACTIONS AFTER TEST (Grams) | | WEIGHT PASSING FINER SIEVE AFTER TEST ACTUAL LOSS (%) | | % PASSING FINER SIEVE AFTER TEST ACTUAL % LOSS | | WEIGHTED AVG CORRECTED PER CENT LOSS | |
| | | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 |
| NO. 4 TO 1 IN. | 30 | 750 | 750 | 650.6 | 662.4 | 99.4 | 87.6 | 13.3 | 11.7 | 6.65 | 5.85 |
| 1 TO 1 IN. | 50 | 1500 | 1500 | 1333.0 | 1324.8 | 8167.0 | 175.2 | 11.1 | 11.7 | 5.55 | 5.85 |
| TOTALS | | 2250 | 2250 | 1983.6 | 1987.4 | 266.4 | 262.8 | 24.4 | 23.4 | 12.20 | 11.70 |
| | | SIEVE WEIGHTED AVG RUNS 1 & 2 | | | | | | 23.90 | | | |

| CONSTITUENT (3500 ft to 7 fm.) | AVG TOTAL WEIGHTED AVG RUNS 1 & 2 12.0 PER CENT | | | | | | | | | | | |
|-----------------------------------|---|-----|--------------------------|-----|----------|-----|---------|-----|--------|-----|-------|-----|
| | NO. OF PARTICLES BEFORE TEST | | NO. PARTICLES AFTER TEST | | | | | | | | | |
| | | | SPLIT | | CRUMBLED | | CRACKED | | FLAKED | | ROUND | |
| | RUN | RUN | RUN | RUN | RUN | RUN | RUN | RUN | RUN | RUN | RUN | RUN |
| Chert | 44 | 42 | 2 | 2 | 4 | 4 | 0 | 0 | 6 | 4 | 32 | 32 |

| FINE AGGREGATE | | | | | | | | | |
|---|---|--|-------|---|-----------|--|--------|--------------------------------------|----------|
| SIZE #EVE CALCU- LATION (in.) | GRADING FOR CALCU- LATION (in.) | WEIGHT OF TEST FRACTIONS BEFORE TEST (Grams) | | WEIGHT OF TEST FRACTIONS AFTER TEST (Grams) | | % PASSING FINER STEVENS ASTEN TEST ACTUAL % LOSS | | WEIGHTED AVERAGE CORRECTED % LOSS | |
| | | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 |
| 3/8-in.-No. 4 | 2 | | | | | (20.7) | (36.8) | 0.4 | 0.3 |
| No. 4-8 | 13 | 100 | 100 | 79.3 | 83.2 | 20.7 | 16.8 | 2.7 | 2.2 |
| No. 8-16 | 20 | 100 | 100 | 94.2 | 92.8 | 5.8 | 7.2 | 1.2 | 1.4 |
| No. 16-30 | 20 | 100 | 100 | 94.8 | 95.6 | 5.2 | 4.4 | 1.0 | 0.9 |
| No. 30-50 | 24 | 100 | 100 | 95.4 | 97.4 | 5.6 | 2.6 | 1.3 | 0.6 |
| No. 50-100 | 14 | - | - | - | - | 0.0 | 0.0 | 0.0 | 0.0 |
| No. 100-PAN | 7 | - | - | - | - | 0.0 | 0.0 | 0.0 | 0.0 |
| TOTALS | 100 | 400 | 400 | 362.7 | 369.0 | 37.3 | 31.0 | 6.6 | 5.4 |
| | | | | SUM WEIGHTED AVG RUNS 1 & 2 | | | | 12.0 | |
| | | | | Avg Total Weighted Avg | Run 1 & 2 | | | 6.0 | Per Cent |

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| SEARCHED BY | J.E.J. | SEARCHED | SLC | |
| FILED BY | J.E.J. | DATE OF REPORT | | |
| COMPUTED | J.E.J. | 11-5-64 | | |

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PLATE 14

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Section B1C

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DATE OF REPORT
3-12-65

PLATE 15

| | | |
|--|---|--|
| FROM: CORPS OF ENGINEERS U. S. ARMY Lower Miss. Valley DIVISION | REPORT OF SOUNDNESS TEST (CRD-C 115) | ADDRESS: USAEEWES, Concrete Division P. O. Drawer 2131 Jackson, Mississippi 39205 |
| SYMBOL VICKS-39 Job 6606 | PROJECT Felsenthal and Calion Locks and Dams | MATERIAL Natural sand and gravel |
| SERIAL NO. VICKS-39 S-3, G-3 | SOURCE Standard Gravel Company, Camden, Ark. | |

| COARSE AGGREGATE | | | | | | | | | | | |
|----------------------------|---|---|-------|--|-------|--|-------|---|-------|--|-------|
| SIEVE SIZE | GRADING FOR CALCULATION (Pv Cen) | WEIGHT OF TEST FRACTION BEFORE TEST - (Grams) | | WEIGHT OF TEST FRACTION AFTER TEST (Grams) | | WEIGHT PASSING FINER SIEVE AFTER TEST ACTUAL LOSS (%) | | % PASSING FINER SIEVE AFTER TEST ACTUAL % LOSS | | WEIGHTED AVG CORRECTED PER CENT LOSS | |
| | | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 |
| NO. 4 TO $\frac{1}{2}$ IN. | 50 | 750 | 750 | 702 | 742 | 48 | 8 | 6.4 | 1.1 | 3.20 | 0.55 |
| $\frac{1}{2}$ TO 1 IN. | 50 | 1500 | 1500 | 1446 | 1419 | 54 | 81 | 3.6 | 5.4 | 1.80 | 2.70 |
| TOTALS | | 2250 | 2250 | 2148 | 2161 | 102 | 89 | 10.0 | 6.5 | 5.00 | 3.25 |
| | | SUM WEIGHTED AVG RUNS 1 & 2 | | | | | | | | 8.25 | |
| | | AVG TOTAL WEIGHTED AVG RUNS 1 & 2 | | | | | | | | 4.1 PER CENT | |

| FINE AGGREGATE | | | | | | | | | |
|----------------|----------------------------|--|-------|---|-------|---|-------|-----------------------------------|----------|
| SIEVE SIZE | GRADING FOR CALCUL. (%) | WEIGHT OF TEST FRACTIONS BEFORE TEST (Grams) | | WEIGHT OF TEST FRACTIONS AFTER TEST (Grams) | | % PASSING FINER SIEVE AFTER TEST ACTUAL % LOSS | | WEIGHTED AVERAGE CORRECTED % LOSS | |
| | | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 |
| 3/8-IN.-NO. 4 | 2 | | | | | (9.2) | (6.6) | 0.2 | 0.1 |
| NO. 4-8 | 13 | 100 | 100 | 90.8 | 93.4 | 9.2 | 6.6 | 1.2 | 0.9 |
| NO. 8-16 | 20 | 100 | 100 | 97.4 | 97.1 | 2.6 | 2.9 | 0.5 | 0.6 |
| NO. 16-30 | 20 | 100 | 100 | 96.5 | 96.3 | 3.5 | 3.7 | 0.7 | 0.7 |
| NO. 30-50 | 24 | 100 | 100 | 97.6 | 98.3 | 4.4 | 1.7 | 1.1 | 0.4 |
| NO. 50-100 | 14 | - | - | - | - | 0.0 | 0.0 | 0.0 | 0.0 |
| NO. 100-PAN | 7 | - | - | - | - | 0.0 | 0.0 | 0.0 | 0.0 |
| TOTALS | 100 | 400 | 400 | 380.3 | 385.1 | 19.7 | 14.9 | 3.7 | 2.7 |
| | | | | SUM WEIGHTED AVG RUNS 1 & 2 | | | | 6.4 | |
| | | | | AVG TOTAL WEIGHTED AVG RUNS 1 & 2 | | | | 3.2 | PER CENT |

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|-----------------------------|----------------------------------|---|--|
| FROM: | CORPS OF ENGINEERS U. S. ARMY | REPORT OF SOUNDNESS TEST (CADC-275) | ADDRESS: USAECWES, Concrete Division P. O. Drawer 2131 Jackson, Mississippi 39205 |
| Lower Miss. Valley DIVISION | | | |

| | | |
|---------------------------------|--|-------------------------------------|
| SYMBOL VICKS-39 Job 6606 | PROJECT Felsenthal and Calion Locks and Dams | MATERIAL Natural sand and gravel |
| SERIAL NO. VICKS-39 S-2, C-2 | SOURCE Monroe Sand and Gravel Company, Sterlington, La. | |

| COARSE AGGREGATE | | | | | | | | | | | |
|--|---|--|-------|---|-------|--|-------|---|-------|--|-------|
| SIEVE SIZE | GRADING FOR CALCULATION (Per Cent) | WEIGHT OF TEST FRACTIONS BEFORE TEST (Grams) | | WEIGHT OF TEST FRACTIONS AFTER TEST (Grams) | | WEIGHT PASSING FINER SIEVE AFTER TEST ACTUAL LOSS (%) | | % PASSING FINER SIEVE AFTER TEST ACTUAL % LOSS | | WEIGHTED AVG CORRECTED PER CENT LOSS | |
| | | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 |
| NO. 4 TO $\frac{1}{2}$ IN. | 50 | 750 | 750 | 745 | 711 | 5 | 39 | 0.7 | 5.2 | 0.35 | 2.60 |
| $\frac{1}{2}$ TO 1 IN. | 50 | 1500 | 1500 | 1470 | 1406 | 30 | 11 | 2.0 | 0.3 | 1.00 | 0.15 |
| TOTALS | | 2250 | 2250 | 2215 | 2207 | 35 | 43 | 2.7 | 5.5 | 1.35 | 2.75 |
| | | | | | | SUM WEIGHTED AVG RUNS 1 & 2 | | 4.1 | | | |
| | | | | | | AVG TOTAL WEIGHTED AVG RUNS 1 & 2 | | 2.0 PER CENT | | | |
| CONSTITUENT (Size $\frac{1}{2}$ in. to 1 in.) | | NO. OF PARTICLES BEFORE TEST | | NO. PARTICLES AFTER TEST | | | | | | | |
| | | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 |
| Chart | | 42 | 43 | 1 | 0 | 0 | 0 | 0 | 0 | 10 | 11 |
| | | | | | | | | | | 42 | 43 |
| | | | | | | | | | | | |

| FINE AGGREGATE | | | | | | | | | | | |
|----------------|--------------------------------------|--|-------|---|-------|---|-------|--------------------------------------|-------|-------|-------|
| SIEVE SIZE | GRADING FOR CALCULATION (%) | WEIGHT OF TEST FRACTIONS BEFORE TEST (Grams) | | WEIGHT OF TEST FRACTIONS AFTER TEST (Grams) | | WEIGHT PASSING FINER SIEVE AFTER TEST ACTUAL % LOSS | | WEIGHTED AVERAGE CORRECTED % LOSS | | | |
| | | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 | RUN 1 | RUN 2 |
| 3/8-IN.-NO. 4 | 2 | - | - | - | - | (9.8) | (5.4) | 0.2 | 0.1 | | |
| NO. 4-8 | 13 | 100 | 100 | 90.2 | 94.6 | 9.8 | 5.4 | 1.3 | 0.7 | | |
| NO. 8-16 | 20 | 100 | 100 | 96.8 | 95.5 | 3.2 | 4.5 | 0.6 | 0.9 | | |
| NO. 16-30 | 20 | 100 | 100 | 97.9 | 97.2 | 2.1 | 2.8 | 0.4 | 0.6 | | |
| NO. 30-50 | 24 | 100 | 100 | 98.1 | 95.7 | 1.9 | 4.3 | 0.5 | 1.0 | | |
| NO. 30-100 | 14 | - | - | - | - | 0.0 | 0.0 | 0.0 | 0.0 | | |
| NO. 100-PAN | 7 | - | - | - | - | 0.0 | 0.0 | 0.0 | 0.0 | | |
| TOTALS | 100 | 400 | 400 | 383.0 | 383.0 | 17.0 | 17.0 | 3.0 | 3.3 | | |
| | | | | | | SUM WEIGHTED AVG RUNS 1 & 2 | | 6.3 | | | |
| | | | | | | AVG TOTAL WEIGHTED AVG RUNS 1 & 2 | | 3.2 PER CENT | | | |

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PLATE 17

Appendix A

Petrographic Report

Samples

1. Five samples of gravel and five samples of natural sand were received for petrographic analysis on 21 August 1964. They represented four deposits of sand and gravel from the central part of southern Arkansas and one deposit of sand and gravel from an area in Louisiana just south of the cities. All of the samples represented processed material taken from stockpiles. Only two of the sands were within the grading limits specified in Corps of Engineers Guide Specifications for Concrete. For the eight samples that were not within the limits, a grading conforming to the middle of that given in the Guide Specifications was assumed for use in calculating sample compositions (table A1-A5). Sample identifications are given below.

| Concrete Division Serial No. | Producer and Source |
|----------------------------------|--|
| VICKS-26 G-1(4), S-1(2) | Ouachita Aggregate Co., Inc., Hampton, Arkansas. Champagnolle Creek Deposit, 4 miles west of Highway 167 between Hampton and El Dorado, Arkansas. |
| VICKS-26 G-2(2), S-2(2) | St. Francis Materials Co., Harrell, Arkansas. Harrell's Pit, 3 miles north of Harrell, Arkansas. |
| VICKS-23 G-1(2); LR-18 S-1(2) | Pine Bluff Sand and Gravel Co., Pine Bluff, Arkansas. 1/4 mile south of Highway 79 on gravel crossroad, approximately 2-1/2 miles west of Bearden, Arkansas. |
| VICKS-39 G-3, S-3 | Standard Gravel Co., Camden, Arkansas. Just north of Camden, Arkansas, north of Highway 79 on Gravel Pit Road. |
| VICKS-39 G-2, S-2 | Monroe Sand and Gravel Co., Sterlington, Louisiana. 1/2 mile west of Sterlington, south on blacktop and gravel road. |

Test procedure

2. A representative portion of each sieve fraction that amounted to five or more percent of a sample was examined. The particles were classified and counted. A stereoscopic microscope was used as needed for the examination of the gravels. Sand sizes larger than the No. 30 sieve were examined with a stereoscopic microscope. The sizes passing No. 30 sieve

were examined as grain immersion mounts with a polarizing microscope. The refractive index of the immersion liquid used was 1.544. A monochromatic sodium light source was used as needed with a microscope equipped with a Saylor double diaphragm in testing for the presence of chalcedonic chert. (Chert having an aggregate refractive index below 1.544 is regarded as chalcedonic chert.) Since each pair of sand and gravel samples came from a common source, the search for chalcedonic chert was restricted to the sand sizes. It was thus assumed that chalcedonic chert is either present or absent in both the sand and the gravel.

Results of examination

3. a. Gravels. All of the gravels are composed largely of blocky chert particles with minor amounts of quartz particles. Dense chert particles make up from 59 to 85 percent of the samples. Particles of vuggy, fractured, or porous chert are present in small to moderate amounts (tables A1-A5).
- b. Sands. The sands are also composed largely of chert and of quartz particles, but quartz is the dominant constituent, amounting to 63 to 73 percent of the total sample (tables A1-A5). Some chalcedonic chert was found in three of the sands. These were VICKS-26 S-1(2), VICKS-39 S-3, and VICKS-39 S-2 (tables A1, A4, and A5, respectively).

Description of constituents

4. a. Dense chert. The particles are blocky with rounded edges, dominantly brown, with many black and light-gray particles.
- b. Porous chert. The porous particles are typically white or tan, tabular in shape with rounded edges, and would be expected to make popouts in concrete surfaces. The particles with porous rims have dense cores and porous rims up to 1/8 in. thick. Dense particles with some porous surface were counted as chert with porous rims. It is not known whether particles with porous rims will form popouts in concrete surfaces. As particle size decreases, the porous particles cannot be separated into "rimmed" and "not rimmed."
- c. Vuggy chert. Particles with many reentrants on their surfaces are classed in this group. They are lost, by breaking into smaller pieces without reentrants, in sizes passing the 3/4-in. sieve. They amounted to from a trace to 8 percent in the samples examined (tables A1-A5).
- d. Fractured chert. The particles contain incipient fractures and are expected to break into smaller pieces in the mixer. They diminish in fractions passing the 3/4-in. sieve. Fractured chert amounted to from a trace to 11 percent in the samples examined (tables A1-A5).

e. Quartz.

(1) Gravels. The particles are blocky with rounded edges and many surface reentrants. They are translucent white to tan with some orange shading. The quartz particles are composed of intergrown quartz crystals, and represent vein quartz surviving longer than the sandstone that originally contained them. A few sandstone fragments contained quartz veins crossing the bedding.

(2) Sands. The quartz particles in the sand are generally transparent single crystals of variable particle shapes and rounded edges.

f. Miscellaneous. Sandstone or quartzite particles make up most of this category in the gravels. The tan sandstone and quartzite are silica-cemented. A few pieces of iron oxide conglomerate are present in the gravels. In the sands many miscellaneous particles are acid igneous rocks.

g. Feldspar. A small amount of blocky pinkish orthoclase and microcline particles were found in VICKS-39 S-2, VICKS-39 S-3, and VICKS-26 S-1(2). No feldspar was found in the other two sands or in the gravels.

Summary

5. Samples from five deposits of sand and gravel have been examined. All represented commercially processed aggregate. Chert made up about 80 to 96 percent of each gravel (tables A1-A5). Most of the chert was dense. The rest of the gravels was largely vein quartz.

6. The sands contained 63 to 73 percent quartz with chert the second most abundant constituent (tables A1-A5). Some chalcedonic chert was found in the samples from the Monroe Sand and Gravel Co. (VICKS-39 S-2), the Standard Gravel Co. (VICKS-39 S-3), and the Ouachita Aggregate Co. (VICKS-26 S-1(2)). Chert in each of these aggregates amounted to more than 20 percent; under the requirements of EM 1110-2-2000 of 15 December 1963, low-alkali cement should be used if any of these aggregates are used.

7. The sand from the Monroe Sand and Gravel Co. was dirty; the larger grains were coated with smaller grains, and the smaller grains were partially coated with reddish clay.

8. Three of the sources, the Ouachita Aggregate Co., the St. Francis Materials Co., and the Fine Bluff Sand and Gravel Co., had been sampled previously, but previous samples were not examined petrographically.

Table A1

Composition of Gravel and Sand from the Ouachita Aggregate Company
near Hampton, Arkansas, VICKS-26 G-1(4), S-1(2)

| <u>Constituents</u> | Composition of Fractions Retained on Sieves | | | | | | Weighted Average Composition, %** | | |
|---------------------|---|----------------|----------------|----------------|--------------------|--------------------|-----------------------------------|--------------------|--------------------|
| | <u>1-in.</u> | <u>3/4-in.</u> | <u>1/2-in.</u> | <u>3/8-in.</u> | <u>No. 1/4-in.</u> | <u>No. 1/8-in.</u> | <u>No. 3/16-in.</u> | <u>No. 1/4-in.</u> | <u>No. 3/8-in.</u> |
| | | | | | | | | | |
| Chert | | | | | | | | | |
| Chalcedonic Dense | 68 | 67 | 73 | 68 | 69 | | | 68 | 71 |
| Vuggy Fractured | 10 | 2 | 2 | 5 | 10 | 11 | | 7 | 1 |
| Porous Rim | 2 | 3 | 3 | 3 | | | | 8 | |
| Porous | 2 | | | | | | | | |
| Quartz | 16 | 17 | 17 | 21 | 20 | 38 | 56 | 71 | 87 |
| Miscellaneous | 2 | 1 | 1 | 1 | 1 | 5 | 2 | 2 | 1 |
| Total | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |

* Based on examination of 300 or more particles in each size shown except the 1-in.; it consisted of 131 particles.

** Percentage calculated using the composition of sieve fractions shown above and a grading taken from the middle of that given in Guide Specifications for Concrete, GE 1401.01, Aug 1963.

† Composed of sandstone, quartzite, and assorted rock fragments.

Table A2

Composition of Gravel and Sand from the St. Francis Materials Company
near Harrell, Arkansas, VICKS-26 G-2(2), S-2(2)

| Constituent | Composition of Fractions Retained on Sieves | | | | | | Weighted Average Composition, %** |
|----------------|---|---------|---------|-----------|-------|--------|-----------------------------------|
| | 3/4-in. | 1/2-in. | 3/8-in. | No. 4-in. | No. 8 | No. 16 | |
| Chert | 70 | 72 | 67 | 74 | 52 | 45 | 24 |
| Dense | | | | | | | 9 |
| Vugs* | | | | | | | 8 |
| Fractured | 2 | 6 | 4 | { 11 | | | 71 |
| Porous rim | 9 | 4 | 8 | | | | |
| Porous | 3 | | | | | | |
| Quartz | 14 | 18 | 20 | 14 | 42 | 54 | 75 |
| Miscellaneous† | 2 | 1 | 1 | 1 | 6 | 1 | 1 |
| Total | 100 | 100 | 100 | 100 | 100 | 100 | 100 |

* Based on the examination of 300 or more particles in each size shown above.

** Percentage calculated using the composition of sieve fractions shown above and a grading taken from the middle of that given in Guide Specifications for Concrete, CE 1401.01, Aug 1963.

† Composed of sandstone, quartzite, and assorted rock particles.

Table A3

Composition of Gravel and Sand from the Pine Bluff Sand and Gravel Company
 Pine Bluff, Arkansas, VICKS-23 G-1(2); LR-18 S-1(2)

| Constituents | Composition of Fractions Retained on Sieves | | | | | | Weighted Average Composition, % | |
|----------------|---|---------|---------|--------------------------|--------|--------|---------------------------------|--|
| | Shown Below, %* | | | No. 3/4-in. to No. 4-in. | | | | |
| | 1-in. | 3/4-in. | 1/2-in. | No. 4-in. | No. 30 | No. 50 | | |
| Chert | 57 | 64 | 73 | 66 | 74 | 65 | 34 | |
| Dense | 1 | 1 | 1 | 1 | 1 | 1 | 1 | |
| Vuggy | 7 | 12 | 5 | 3 | 9 | 19 | 12 | |
| Fractured | 17 | 12 | 5 | 9 | 19 | 30 | 19 | |
| Porous rim | 9 | 9 | 9 | 9 | 9 | 9 | 9 | |
| Porcous | | | | | | | | |
| Quartz | 19 | 12 | 9 | 14 | 14 | 29 | 33 | |
| Miscellaneous† | | 1 | Trace | 1 | Trace | 6 | 4 | |
| | 100 | 100 | 100 | 100 | 100 | 100 | 100 | |

* Based on examination of 300 or more particles in each fraction shown except the 1-in.; it consisted of 108 particles.

** Percentage calculated using the composition of sieve fractions shown above and a grading taken from the middle of that given in Guide Specifications for Concrete, CE 1401.01, Aug. 1963.

+ Percentage based on the composition by sieve fractions and on the grading of the sample. For this calculation the small amount of sample not examined was assumed to have the composition of the adjoining size.

†† Composed of sandstone, quartzite, and unsorted rock particles.

Table A4

Composition of Gravel and Sand from the Standard Gravel Company
Camden, Arkansas; VICKS-39 G-3, S-3

| Constituent ^a | Composition of Fractions Retained on Sieved Screens Below, %* | | | | | | Weighted Average Composition, %** | | | | |
|--------------------------|--|-------------|-------------|-------------|-----------|-----------|--------------------------------------|------------|-----------------------------------|---------------------------------|------|
| | 1- in. | 3/4- in. | 1/2- in. | 3/8- in. | No. 16 | No. 30 | No. 50 | No. 100 | No. 1/4-in. to 1-1/2-in. | No. 1/4-in. to 3/4-in. | Sand |
| | in. | in. | in. | in. | in. | in. | in. | in. | in. | in. | in. |
| Chert | | | | | | | | | | | 27 |
| Quartzite | 72 | 82 | 87 | 69 | 81 | | | | | | |
| Dense | | | Trace | | | | | | | | |
| Vuggy | | 1 | 7 | | | | | | | | |
| Fractured | 13 | 4 | 5 | 5 | | | | | | | |
| Folrous | 6 | | 7 | 6 | 13 | 23 | 49 | 77 | 86 | 91 | 7 |
| Quartz | 7 | 6 | 7 | 6 | | | | | | | |
| Miscellaneous | 1 | 1 | 1 | 1 | 1 | 4 | 6 | 3 | 6 | 2 | 1 |
| Total | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |

- * Based on enumeration of 300 or more particles in each size shown except the 1-in.; it consisted of 94 particles.
- ** Percentage calculated using the composition of sieve fractions shown above and a grading taken from the middle of that given in Guide Specifications for Concrete, CE 1101.01, Aug 1963.
- ^a Composed of sandstone, quartzite, and eozero rock fragments.

Table A5

Composition of Gravel and Sand from the Monroe Sand and Gravel Company
Sterlington, Louisiana, VICKS-39 G-2, S-2

| constituents | Composition of Fractions Retained on Sieves Shown Below, %* | | | | | | | Weighted Average Composition, % | | |
|----------------|--|-------------|-------------|-------------|-----------------|---------------|-------------------------|------------------------------------|---------------------|-----------------|
| | 1-1/2- in. | 3/4- in. | 1/2- in. | 3/8- in. | No. 4 Gravel | No. 4 Sand | No. 8 16 30 50 | No. 16 30 50 100 | No. 1-1/2- in.** | No. 4- in.** |
| Chert | | | | | | | 79 | 52 | 33 | 5 |
| Chalcedonic | | | | | | | 2 | 8 | 2 | 21 |
| Dense | 58 | 79 | 89 | 79 | 75 | 76 | | | | |
| Vuggy | 24 | 10 | 3 | 3 | | | | | | |
| Fractured | 8 | 4 | 1 | 1 | | | | | | |
| Porous rim | | 3 | 4 | 10 | 10 | 11 | | | | |
| Porous | | | | | | | | | | |
| Quartz | 1 | 3 | 10 | 12 | 19 | 41 | 60 | 93 | 83 | 70 |
| Miscellaneous† | 10 | 3 | 3 | 1 | 1 | 3 | 6 | 4 | 1 | 6 |
| Feldspar | | | | | | | 1 | 3 | 1 | 3 |
| Total | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |

* Based on examination of 300 or more particles in each sieve fraction shown except the 1-1/2-in. and the No. 4 of the sand; the 1-1/2-in. size consisted of 50 particles, and the No. 4 size of the sand contained 88 particles.

** Percentage calculated using the composition of sieve fractions shown above and a grading taken from the middle of that given in Guide Specifications for Concrete, CE 1401.01, Aug 1963.

† Percentage based on the composition by sieve fractions and on the grading of the sample. The material passing No. 100 sieve was assumed to have a composition like the No. 100 sieve size material for this calculation.

†† Composed of sandstone, quartzite, and assorted rock particles.